

# 1.5 GHz Ultrahigh Speed Op Amp

# AD8000

#### **FEATURES**

High speed

1.5 GHz, -3 dB bandwidth (G = +1) 650 MHz, full power bandwidth (G = +2, V<sub>0</sub> = 2 V p-p) Slew rate: 4100 V/µs 0.1% settling time: 12 ns **Excellent video specifications** 0.1 dB flatness: 170 MHz Differential gain: 0.02% Differential phase: 0.01° Output overdrive recovery: 22 ns Low noise: 1.6 nV/ $\sqrt{Hz}$  input voltage noise Low distortion over wide bandwidth 75 dBc SFDR @ 20 MHz 62 dBc SFDR @ 50 MHz Input offset voltage: 1 mV typ High output current: 100 mA Wide supply voltage range: 4.5 V to 12 V Supply current: 13.5 mA **Power-down mode** 

#### APPLICATIONS

Professional video High speed instrumentation Video switching IF/RF gain stage CCD imaging 勝特力材料 886-3-5753170 胜特力电子(上海) 86-21-34970699 胜特力电子(深圳) 86-755-83298787 Http://www.100y.com.tw

#### **GENERAL DESCRIPTION**

The AD8000 is an ultrahigh speed, high performance, current feedback amplifier. Using ADI's proprietary eXtra Fast Complementary Bipolar (XFCB) process, the amplifier can achieve a small signal bandwidth of 1.5 GHz and a slew rate of 4100 V/µs.

The AD8000 has low spurious-free dynamic range (SFDR) of 75 dBc @ 20 MHz and input voltage noise of 1.6 nV/ $\sqrt{Hz}$ . The AD8000 can drive over 100 mA of load current with minimal distortion. The amplifier can operate on +5 V to ±6 V. These specifications make the AD8000 ideal for a variety of applications, including high speed instrumentation.

With a differential gain of 0.02%, differential phase of 0.01°, and 0.1 dB flatness out to 170 MHz, the AD8000 has excellent video specifications, which ensure that even the most demanding video systems maintain excellent fidelity.

#### Rev. A

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#### CONNECTION DIAGRAMS

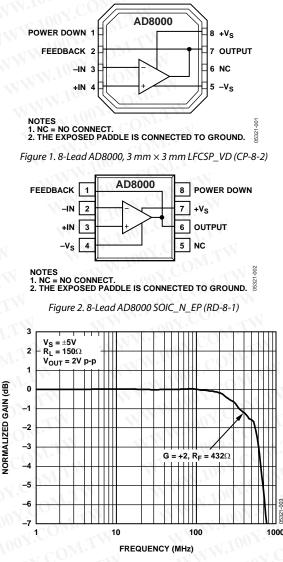


Figure 3. Large Signal Frequency Response

The AD8000 power-down mode reduces the supply current to 1.3 mA. The amplifier is available in a tiny 8-lead LFCSP package, as well as in an 8-lead SOIC package. The AD8000 is rated to work over the extended industrial temperature range ( $-40^{\circ}$ C to +125°C). A triple version of the AD8000 (AD8003) is underdevelopment.

 One Technology Way, P.O. Box 9106, Norwood, MA 02062-9106, U.S.A.

 Tel: 781.329.4700
 www.analog.com

 Fax: 781.461.3113
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# REVISION HISTORY

REVISION HISTORY	
3/10—Rev. 0 to Rev. A	
Changes to Figure 1 and Figure 2	
Changes to Table 3	
Updated Outline Dimensions and Changes to	
Ordering Guide	
1/05—Rev. 0: Initial Version	

# WWW.100Y.COM.TW 1/05—Rev. 0: Initial Version WWW.100Y.COM.TW

### SPECIFICATIONS WITH ±5 V SUPPLY

At  $T_A = 25^{\circ}$ C,  $V_S = \pm 5$  V,  $R_L = 150 \Omega$ , Gain = +2,  $R_F = R_G = 432 \Omega$ , unless otherwise noted. Exposed paddle should be connected to WWW.100 1100X.COM.7 W100Y.COM. ground. MT.MO WT.M

M.TW

Table 1.
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Parameter	Conditions	Min	Тур	Max	Unit
DYNAMIC PERFORMANCE	CONT.	AN.COM	WT.		T
–3 dB Bandwidth	$G = +1$ , $V_0 = 0.2 V p-p$ , SOIC/LFCSP	CON	1580/1350		MHz
	$G = +2$ , $V_0 = 2 V p-p$ , SOIC/LFCSP	1004.00	650/610		MHz
Bandwidth for 0.1 dB Flatness	$V_0 = 2 V p-p$ , SOIC/LFCSP	. V.CO	190/170		MHz
Slew Rate	$G = +2$ , $V_0 = 4$ V step	N.100 1.	4100		V/µs
Settling Time to 0.1%	$G = +2, V_0 = 2 V step$	1004.0	12		ns
NOISE/HARMONIC PERFORMANCE	NW NON	V.	WT		
Second/Third Harmonic	$V_0 = 2 V p-p, f = 5 MHz, LFCSP only$	N.100	86/89		dBc
Second/Third Harmonic	$V_0 = 2 V p-p$ , f = 20 MHz, LFCSP only	100%	75/79		dBc
Input Voltage Noise	f = 100 kHz	NN. ANDY	1.6		nV/√H:
Input Current Noise	f = 100 kHz, –IN	W.100	26		pA/√H
M. ONY.CO. TW W	f = 100 kHz, +IN	100	3.4		pA/√H
Differential Gain Error	NTSC, $G = +2$	WWW.	0.02		%
Differential Phase Error	NTSC, $G = +2$	L.W.W.	0.01		Degree
DC PERFORMANCE			1002.001	<u>TN</u>	Deg.ee
Input Offset Voltage	WWW.LCOM. TW	WWW.	LOY.COM	10	mV
Input Offset Voltage Drift	W.100 COM.I	WW		10	μV/°C
Input Bias Current (Enabled)	+Ι <sub>β</sub> 100Υ.Ο.Ο.Μ.ΤΥ		-5	+4	μΑ
input blas current (Enabled)	-IB WW. COMPANY	WW	-3	+45	μΑ
Transimpedance	-B COM.I	570	890	1600	kΩ
INPUT CHARACTERISTICS	NI 1002. ON TH	570	0,0	1000	132
Noninverting Input Impedance	WWW. SOV.COM TW	W	2/3.6		MΩ/pF
Input Common-Mode Voltage Range	W.IVO COM.	1	-3.5 to +3.5		V
Common-Mode Rejection Ratio	$V_{CM} = \pm 2.5 V$	-52	-5.5 t0 +5.5 -54	-56	dB
Overdrive Recovery	G = +1, f = 1 MHz, triangle wave	-J2	30		
POWER DOWN PIN	G = +1, 1 = 1 MHz, thangle wave		30	<del>J CO</del>	ns
	Power-down	TW	111 2110		
Power-Down Input Voltage		W	< +Vs - 3.1		V
Turn-Off Time	Enabled	1.	> +Vs - 1.9		U-1
Turn-Oπ Time	50% of power-down voltage to 10% of V <sub>OUT</sub> final, $V_{IN} = 0.3$ V p-p	VI.T.W	150		ns
Turn-On Time	50% of power-down voltage to	WTI	300		ns
rum on nine	90% of $V_{OUT}$ final, $V_{IN} = 0.3 \text{ V p-p}$	DIT.	500		COM
Input Bias Current	N.TN W 1001.	M.L			100
Enabled	TW WWW 100Y.	-1.1	+0.17	+1.4	μA
Power-Down	MILL WWW.IC.	-300	-235	-160	μΑ
OUTPUT CHARACTERISTICS	N.1. W.1001	-ON		N.W.M	-16
Output Voltage Swing	$R_L = 100 \Omega$	±3.7	±3.9		V
Output Voltage Swing	$R_L = 1 k\Omega$	±3.9	±4.1		v
Linear Output Current	$V_0 = 2 V p-p$ , second HD < -50 dBc	M.COM.	100		mA
Overdrive Recovery	G = + 2, $f = 1$ MHz, triangle wave	1012.00	45		ns
	$G = +2$ , $V_{IN} = 2.5$ V to 0 V step	V.COM	22		ns
POWER SUPPLY		TOP - COD			
Operating Range	NTW WWW	4.5		12	V.10
Quiescent Current	N.COM. WWW	12.7	13.5	14.3	mA
Quiescent Current (Power-Down)	In ONLIN.	1.1	1.3	14.5	mA
	–PSRR/+PSRR	-56/-61	-59/-63	1.05	dB
Power Supply Rejection Ratio		-n/-n			IUD

### **SPECIFICATIONS WITH +5 V SUPPLY**

At  $T_A = 25^{\circ}$ C,  $V_S = +5$  V,  $R_L = 150 \Omega$ , Gain = +2,  $R_F = R_G = 432 \Omega$ , unless otherwise noted. Exposed paddle should be connected to WWW.100 4.100Y.COM.T W100Y.COM ground. WT.MO WT.Mo

#### Table 2.

Parameter	Conditions	Min	Тур	Max	Unit
DYNAMIC PERFORMANCE	CONT.	· CO	M.		
–3 dB Bandwidth	$G = +1, V_0 = 0.2 V p-p$	100 1.	980		MHz
	$G = +2, V_0 = 2 V p - p$	100Y.C	477		MHz
	$G = +10, V_0 = 0.2 V p-p$	V.LO	328		MHz
Bandwidth for 0.1 dB Flatness	$V_0 = 0.2 V p - p$	W.100 1.	136		MHz
	$V_0 = 2 V p - p$	1001	136		MHz
Slew Rate	$G = +2, V_0 = 2 V step$	WW.10	2700		V/µs
Settling Time to 0.1%	$G = +2, V_0 = 2 V step$	.100	16		ns
NOISE/HARMONIC PERFORMANCE				N	115
Second/Third Harmonic	$V_0 = 2 V p-p$ , 5 MHz, LFCSP only	WWW.L	71/71		dBc
Second/Third Harmonic	$V_0 = 2 V p p$ , $3 M Hz$ , $LFCSP$ only	I.W.I	60/62		dBc
Input Voltage Noise	f = 100  kHz	MM	1.6		nV/√Hz
	f = 100  kHz f = 100  kHz, -IN	WW			nv/√Hz pA/√Hz
Input Current Noise			26		
COMPANY CONTRACT	f = 100  kHz, +IN	WW	3.4		pA/√Hz
Differential Gain Error	NTSC, $G = +2$		0.01		%
Differential Phase Error	NTSC, $G = +2$	N.	0.06	TIM	Degree
DC PERFORMANCE	WWW. LOW.COM TW	W			N
Input Offset Voltage	COM. 1		1.3	10	mV
Input Offset Voltage Drift	WW 100Y.COM.TW		18		μV/°C
Input Bias Current (Enabled)	+lB WWW.reav.Com	× ×	-5	+3	μA
	-I <sub>B</sub>		-1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1	+45	μA
Transimpedance	WW 100Y.CONT	440	800	1500	kΩ
INPUT CHARACTERISTICS	WWW.	W	WWW	N.C	WTA
Noninverting Input Impedance	WW.100 COM		2/3.6		MΩ/pF
Input Common-Mode Voltage Range	WWW 100Y.Com	TW	1.5 to 3.6		V
Common-Mode Rejection Ratio	$V_{CM} = \pm 2.5 V$	-51	-52	-54	dB
Overdrive Recovery	G = +1, $f = 1$ MHz, triangle wave	1.1	60		ns
POWER DOWN PIN	TW W 1001.	N.T.Y	W.	1003	-M.I
Power-Down Input Voltage	Power-down	WT	< +Vs - 3.1		V
W 1001. CO	Enable	OM. Y	> +Vs - 1.9		V COM
Turn-Off Time	50% of power-down voltage to 10% of $V_{OUT}$ final, $V_{IN} = 0.3 V p-p$	COM.TW	200		ns
Turn-On Time	50% of power-down voltage to	- COM-1	300		ns
	90% of $V_{OUT}$ final, $V_{IN} = 0.3 \text{ V} \text{ p-p}$	T.M.			1001.
Input Current	CONTRACT NWN.1	N.COME			LOOY.CL
Enabled	COM.1	-1.10M	+0.17	+1.4	μA
Power-Down	WITH WITH	-50	-40	-30	μA
OUTPUT CHARACTERISTICS	WWWWWWWWWWWW	ANY.COX	WT .	MM	Your.
Output Voltage Swing	$R_L = 100 \Omega$	1.1 to 3.9	1.05 to 4.1		V
WW I	$R_L = 1 k\Omega$	1 to 3.1	0.85 to 4.15		V-100
Linear Output Current	$V_0 = 2 V p-p$ , second HD < -50 dBc	J.Vool	70		mA
Overdrive Recovery	G = +2, $f = 100$ kHz, triangle wave	1.100 - C	65		ns
POWER SUPPLY		N 100 Y.C	MTN		I.W.
Operating Range	T COMP. THE WY	4.5		12	V
Quiescent Current	1.100 COM. 1.	11	12	13	mA
Quiescent Current (Power-Down)	W WT W	0.7 100	0.95	1.25	mA
				1.23	
Power Supply Rejection Ratio	-PSRR/+PSRR	-55/-60	-57/-62		dB

### **ABSOLUTE MAXIMUM RATINGS**

#### Table 3.

10010 01	
Parameter	Rating
Supply Voltage	12.6 V
Power Dissipation	See Figure 4
Common-Mode Input Voltage	$-V_{s} - 0.7 V$ to $+V_{s} + 0.7 V$
Differential Input Voltage	±Vs
Storage Temperature	–65°C to +125°C
Operating Temperature Range	-40°C to +125°C
Lead Temperature Range (Soldering, 10 sec)	300°C
Junction Temperature	150°C

Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### THERMAL RESISTANCE

 $\theta_{JA}$  is specified for the worst-case conditions, that is,  $\theta_{JA}$  is specified for device soldered in the circuit board for surface-mount packages.

Table 4. Thermal Resistance

Package Type	θյΑ	οıθ	Unit
SOIC-8	80	30	°C/W
3 mm × 3 mm LFCSP	93	35	°C/W

#### Maximum Power Dissipation

The maximum safe power dissipation for the AD8000 is limited by the associated rise in junction temperature ( $T_J$ ) on the die. At approximately 150°C, which is the glass transition temperature, the properties of the plastic change. Even temporarily exceeding this temperature limit can change the stresses that the package exerts on the die, permanently shifting the parametric performance of the AD8000. Exceeding a junction temperature of 175°C for an extended period of time can result in changes in silicon devices, potentially causing degradation or loss of functionality. The power dissipated in the package  $(P_D)$  is the sum of the quiescent power dissipation and the power dissipated in the die due to the AD8000 drive at the output. The quiescent power is the voltage between the supply pins  $(V_S)$  times the quiescent current  $(I_S)$ .

 $P_D$  = Quiescent Power + (Total Drive Power – Load Power)

$$P_{D} = \left(V_{S} \times I_{S}\right) + \left(\frac{V_{S}}{2} \times \frac{V_{OUT}}{R_{L}}\right) - \frac{V_{OUT}^{2}}{R_{L}}$$

RMS output voltages should be considered. If  $R_L$  is referenced to  $-V_s$ , as in single-supply operation, the total drive power is  $V_s \times I_{OUT}$ . If the rms signal levels are indeterminate, consider the worst case, when  $V_{OUT} = V_s/4$  for  $R_L$  to midsupply.

$$P_D = \left(V_S \times I_S\right) + \frac{\left(V_S/4\right)^2}{R_I}$$

In single-supply operation with  $R_L$  referenced to  $-V_S$ , worst case is  $V_{OUT} = V_S/2$ .

Airflow increases heat dissipation, effectively reducing  $\theta_{JA}$ . Also, more metal directly in contact with the package leads and exposed paddle from metal traces, through holes, ground, and power planes reduces  $\theta_{JA}$ .

Figure 4 shows the maximum safe power dissipation in the package vs. the ambient temperature for the exposed paddle SOIC (80°C/W) and the LFCSP (93°C/W) package on a JEDEC standard 4-layer board.  $\theta_{JA}$  values are approximations.

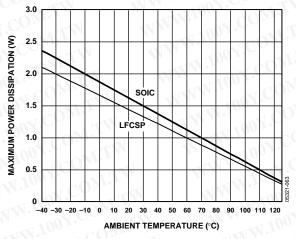


Figure 4. Maximum Power Dissipation vs. Temperature for a 4-Layer Board

#### **ESD CAUTION**

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although this product features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation and loss of functionality.



# **TYPICAL PERFORMANCE CHARACTERISTICS**

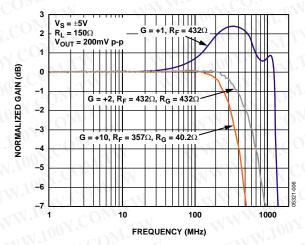


Figure 5. Small Signal Frequency Response vs. Various Gains

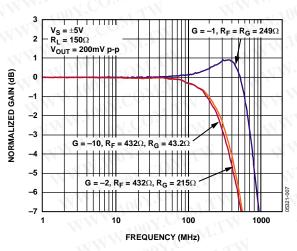


Figure 6. Small Signal Frequency Response vs. Various Gains

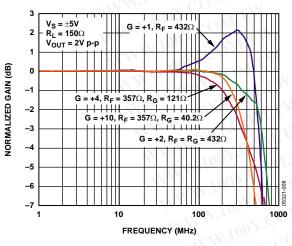


Figure 7. Large Signal Frequency Response vs. Various Gains

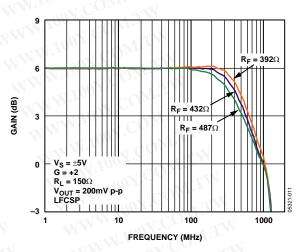


Figure 8. Small Signal Frequency Response vs. R<sub>F</sub>

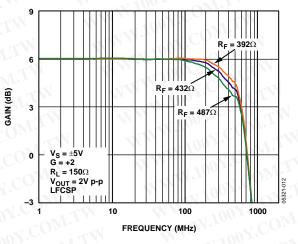


Figure 9. Large Signal Frequency Response vs. R<sub>F</sub>

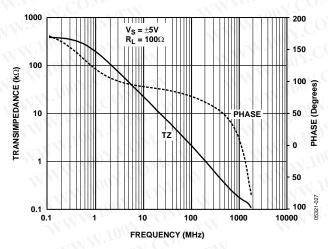


Figure 10. Transimpedance and Phase vs. Frequency

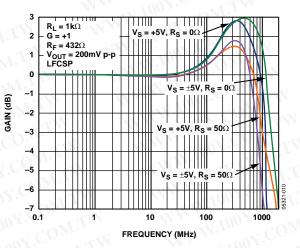


Figure 11. Small Signal Frequency Response vs. Supply Voltage

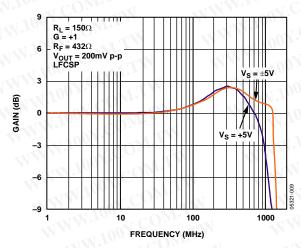


Figure 12. Small Signal Frequency Response vs. Supply Voltage

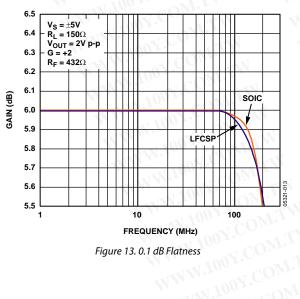


Figure 13. 0.1 dB Flatness WWW.100Y.COM.

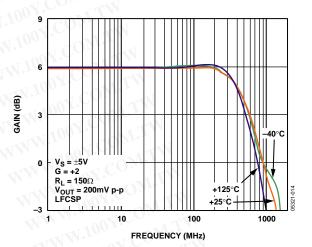


Figure 14. Small Signal Frequency Response vs. Temperature

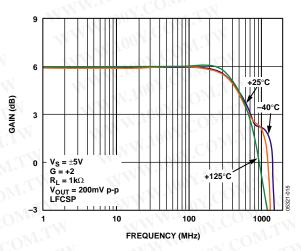
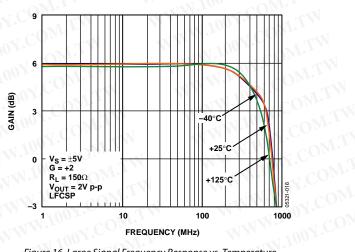


Figure 15. Small Signal Frequency Response vs. Temperature





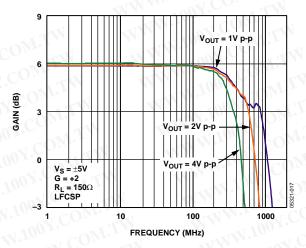


Figure 17. Large Signal Frequency Response vs. Various Outputs

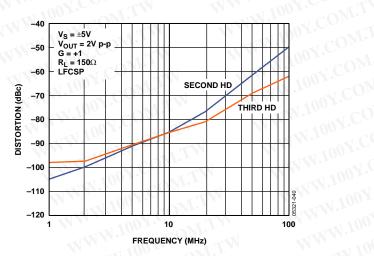


Figure 18. Harmonic Distortion vs. Frequency

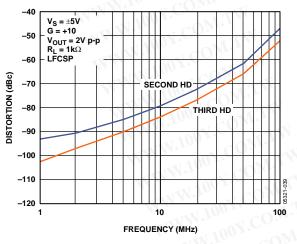
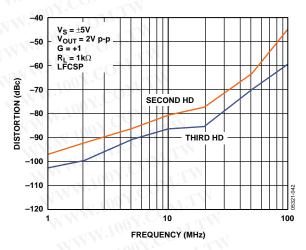
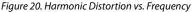
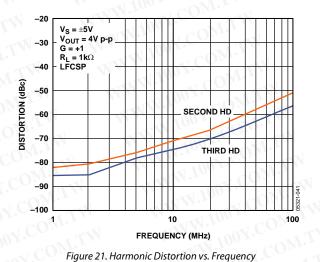
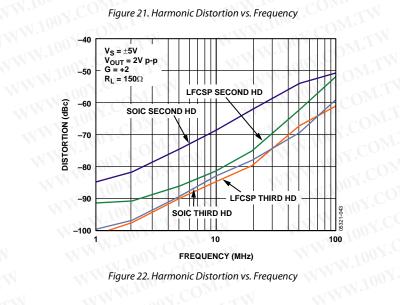


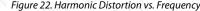
Figure 19. Harmonic Distortion vs. Frequency WWW.100Y.COM











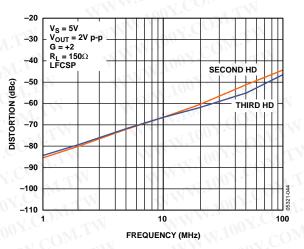
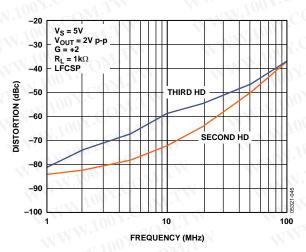


Figure 23. Harmonic Distortion vs. Frequency





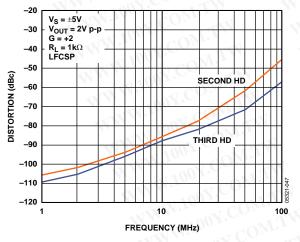


Figure 25. Harmonic Distortion vs. Frequency

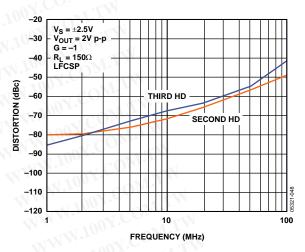


Figure 26. Harmonic Distortion vs. Frequency

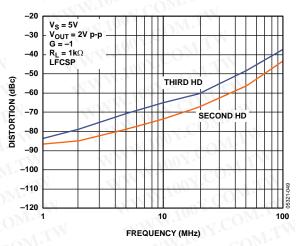


Figure 27. Harmonic Distortion vs. Frequency

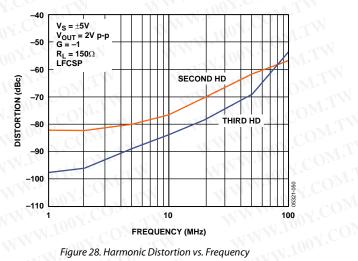


Figure 28. Harmonic Distortion vs. Frequency

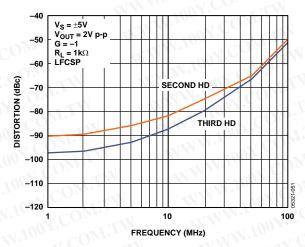


Figure 29. Harmonic Distortion vs. Frequency

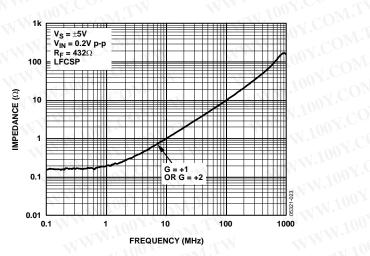


Figure 30. Output Impedance vs. Frequency

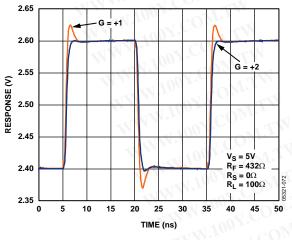


Figure 31. Small Signal Transient Response WWW.100Y.COM

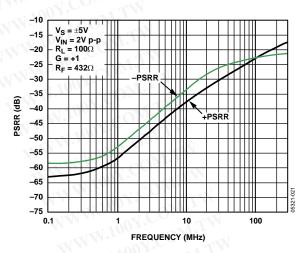


Figure 32. Power Supply Rejection Ratio (PSRR) vs. Frequency

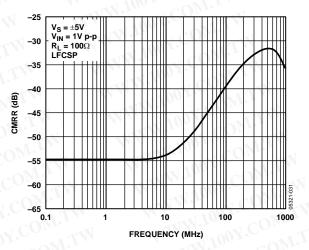
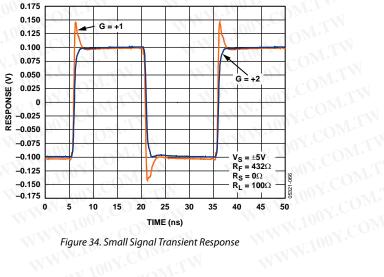
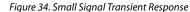
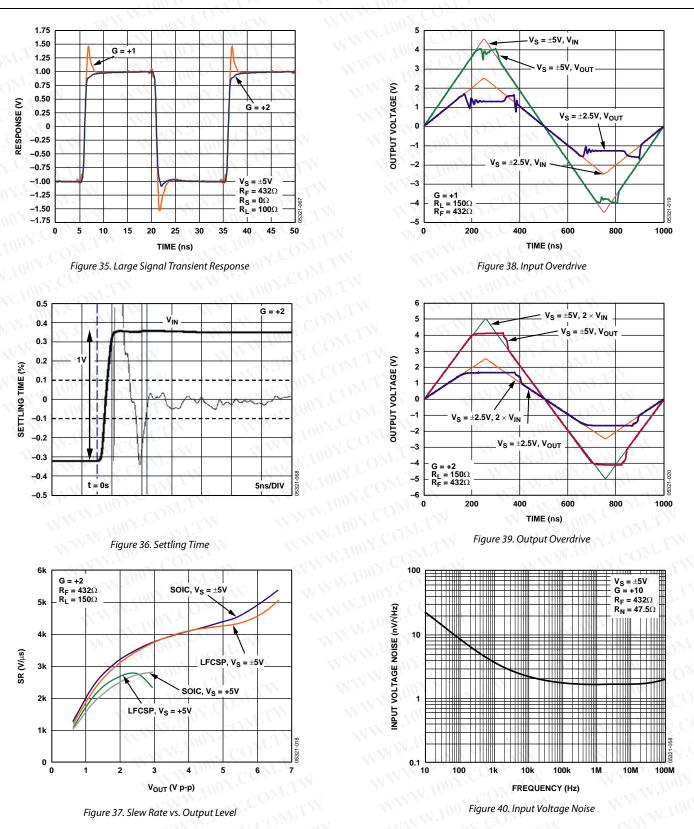


Figure 33. Common-Mode Rejection Ratio vs. Frequency







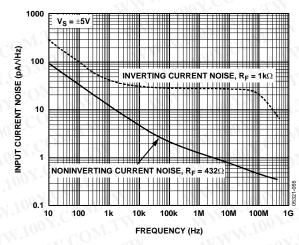


Figure 41. Input Current Noise

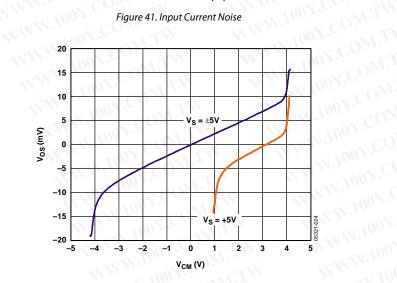


Figure 42. Input Vos vs. Common-Mode Voltage

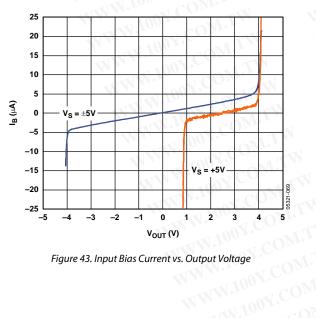


Figure 43. Input Bias Current vs. Output Voltage

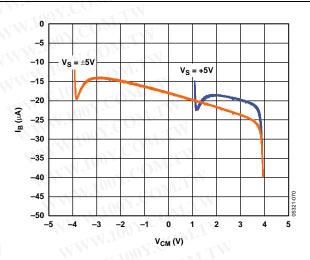


Figure 44. Input Bias Current vs. Common-Mode Voltage

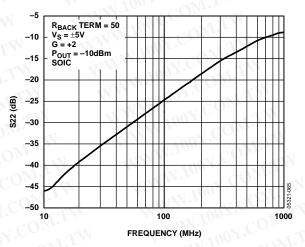


Figure 45. Output Voltage Standing Wave Ratio (S22)

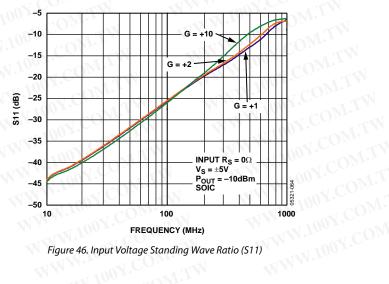
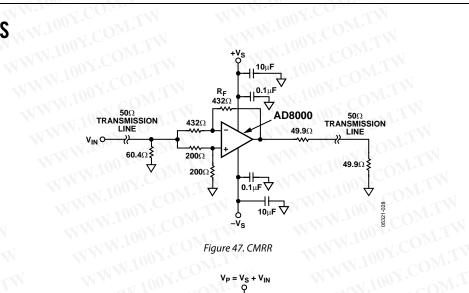


Figure 46. Input Voltage Standing Wave Ratio (S11)

# **TEST CIRCUITS**

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Figure 47. CMRR

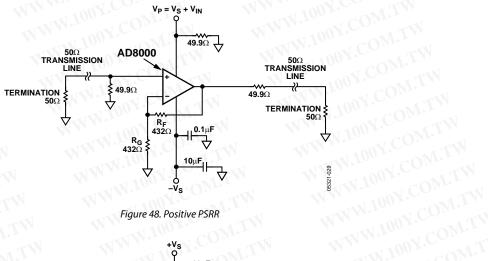


Figure 48. Positive PSRR

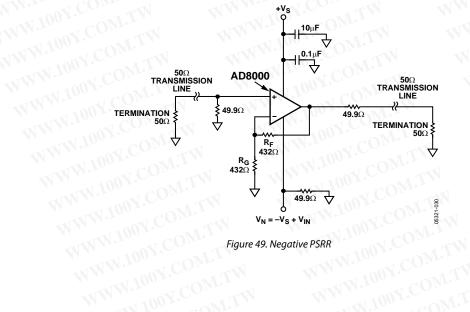


Figure 49. Negative PSRR

### **APPLICATIONS**

All current feedback amplifier operational amplifiers are affected by stray capacitance at the inverting input pin. As a practical consideration, the higher the stray capacitance on the inverting input to ground, the higher  $R_F$  needs to be to minimize peaking and ringing.

#### **CIRCUIT CONFIGURATIONS**

Figure 50 and Figure 51 show typical schematics for noninverting and inverting configurations. For current feedback amplifiers, the value of feedback resistance determines the stability and bandwidth of the amplifier. The optimum performance values are shown in Table 5 and should not be deviated from by more than  $\pm 10\%$  to ensure stable operation. Figure 8 shows the influence varying R<sub>F</sub> has on bandwidth. In noninverting unity-gain configurations, it is recommended that an R<sub>s</sub> of 50  $\Omega$  be used, as shown in Figure 50.

Table 5 provides a quick reference for the circuit values, gain, and output voltage noise.

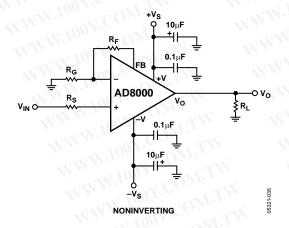


Figure 50. Noninverting Configuration

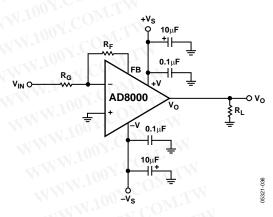


Figure 51. Inverting Configuration

#### **VIDEO LINE DRIVER**

The AD8000 is designed to offer outstanding performance as a video line driver. The important specifications of differential gain (0.02%), differential phase (0.01°), and 650 MHz bandwidth at 2 V p-p meet the most exacting video demands. Figure 52 shows a typical noninverting video driver with a gain of +2.

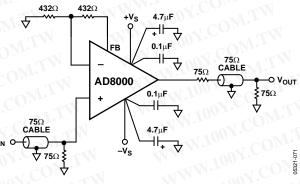


Figure 52. Video Line Driver

Gain	Component Values (Ω)			-3 dB SS -3 dB LS Bandwidth Bandwidth (MHz) (MHz)			Slew Rate (V/µsec)	Output Noise (nV/√Hz)	Total Output Noise Including Resistors (nV/√Hz)
	RF	Rg	LFCSP	SOIC	LFCSP	SOIC	.10	CON.	WW.IO
1	432		1380	1580	550	600	2200	10.9	11.2
2	432	432	600	650	610	650	3700	11.3	11.9
4	357	120	550	550	350	350	3800	10	12
10	357	40	350	365	370	370	3200	18.4	19.9

#### Table 5. Typical Values (LFCSP/SOIC)

#### LOW DISTORTION PINOUT

The AD8000 LFCSP features ADI's new low distortion pinout. The new pinout lowers the second harmonic distortion and simplifies the circuit layout. The close proximity of the noninverting input and the negative supply pin creates a source of second harmonic distortion. Physical separation of the noninverting input pin and the negative power supply pin reduces this distortion significantly, as seen in Figure 22.

By providing an additional output pin, the feedback resistor can be connected directly across Pin 2 and Pin 3. This greatly simplifies the routing of the feedback resistor and allows a more compact circuit layout, which reduces its size and helps to minimize parasitics and increase stability.

The SOIC also features a dedicated feedback pin. The feedback pin is brought out on Pin 1, which is typically a No Connect on standard SOIC pinouts.

Existing applications that use the standard SOIC pinout can take full advantage of the performance offered by the AD8000. For drop-in replacements, ensure that Pin 1 is not connected to ground or to any other potential because this pin is connected internally to the output of the amplifier. For existing designs, Pin 6 can still be used for the feedback resistor.

#### **EXPOSED PADDLE**

The AD8000 features an exposed paddle, which can lower the thermal resistance by 25% compared to a standard SOIC plastic package. The paddle can be soldered directly to the ground plane of the board. Figure 53 shows a typical pad geometry for the LFCSP, the same type of pad geometry can be applied to the SOIC package.

Thermal vias or "heat pipes" can also be incorporated into the design of the mounting pad for the exposed paddle. These additional vias improve the thermal transfer from the package to the PCB. Using a heavier weight copper on the surface to which the amplifier's exposed paddle is soldered also reduces the overall thermal resistance "seen" by the AD8000.

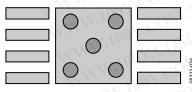


Figure 53. LFCSP Exposed Paddle Layout

#### PRINTED CIRCUIT BOARD LAYOUT

Laying out the printed circuit board (PCB) is usually the last step in the design process and often proves to be one of the most critical. A brilliant design can be rendered useless because of a poor or sloppy layout. Since the AD8000 can operate into the  $R_F$  frequency spectrum, high frequency board layout considerations must be taken into account. The PCB layout, signal routing, power supply bypassing, and grounding all must be addressed to ensure optimal performance.

#### **SIGNAL ROUTING**

The AD8000 LFCSP features the new low distortion pinout with a dedicated feedback pin and allows a compact layout. The dedicated feedback pin reduces the distance from the output to the inverting input, which greatly simplifies the routing of the feedback network.

To minimize parasitic inductances, ground planes should be used under high frequency signal traces. However, the ground plane should be removed from under the input and output pins to minimize the formation of parasitic capacitors, which degrades phase margin. Signals that are susceptible to noise pickup should be run on the internal layers of the PCB, which can provide maximum shielding.

#### **POWER SUPPLY BYPASSING**

Power supply bypassing is a critical aspect of the PCB design process. For best performance, the AD8000 power supply pins need to be properly bypassed.

A parallel connection of capacitors from each of the power supply pins to ground works best. Paralleling different values and sizes of capacitors helps to ensure that the power supply pins "see" a low ac impedance across a wide band of frequencies. This is important for minimizing the coupling of noise into the amplifier. Starting directly at the power supply pins, the smallest value and sized component should be placed on the same side of the board as the amplifier, and as close as possible to the

amplifier, and connected to the ground plane. This process should be repeated for the next larger value capacitor. It is recommended for the AD8000 that a 0.1  $\mu$ F ceramic 0508 case be used. The 0508 offers low series inductance and excellent high frequency performance. The 0.1  $\mu$ F case provides low impedance at high frequencies. A 10  $\mu$ F electrolytic capacitor should be placed in parallel with the 0.1  $\mu$ F. The 10  $\mu$ f capacitor provides low ac impedance at low frequencies. Smaller values of electrolytic capacitors can be used, depending on the circuit requirements. Additional smaller value capacitors help to provide a low impedance path for unwanted noise out to higher frequencies but are not always necessary.

Placement of the capacitor returns (grounds), where the capacitors enter into the ground plane, is also important. Returning the capacitors grounds close to the amplifier load is critical for distortion performance. Keeping the capacitors distance short, but equal from the load, is optimal for performance.

In some cases, bypassing between the two supplies can help to improve PSRR and to maintain distortion performance in crowded or difficult layouts. This is as another option to improve performance.

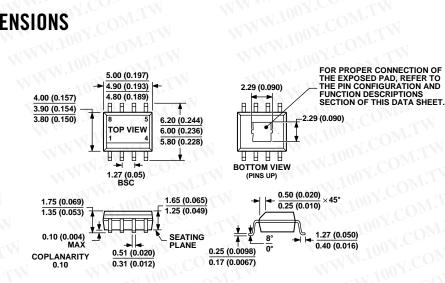
Minimizing the trace length and widening the trace from the capacitors to the amplifier reduce the trace inductance. A series inductance with the parallel capacitance can form a tank circuit, which can introduce high frequency ringing at the output. This additional inductance can also contribute to increased distortion due to high frequency compression at the output. The use of vias should be minimized in the direct path to the amplifier power supply pins since vias can introduce parasitic inductance, which can lead to instability. When required, use multiple large diameter vias because this lowers the equivalent parasitic inductance.

#### GROUNDING

The use of ground and power planes is encouraged as a method of proving low impedance returns for power supply and signal currents. Ground and power planes can also help to reduce stray trace inductance and to provide a low thermal path for the amplifier. Ground and power planes should not be used under any of the pins of the AD8000. The mounting pads and the ground or power planes can form a parasitic capacitance at the amplifiers input. Stray capacitance on the inverting input and the feedback resistor form a pole, which degrades the phase margin, leading to instability. Excessive stray capacitance on the output also forms a pole, which degrades phase margin.

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#### **OUTLINE DIMENSIONS**



COMPLIANT TO JEDEC STANDARDS MS-012-A A CONTROLLING DIMENSIONS ARE IN MILLIMETER; INCH DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

100Y.COM.TW Figure 54. 8-Lead Standard Small Outline Package, with Exposed Pad [SOIC\_N\_EP] Narrow Body (RD-8-1) Dimensions shown in millimeters and (inches)

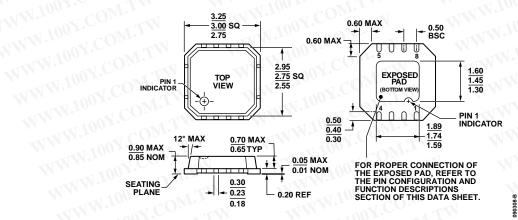


Figure 55. 8-Lead Lead Frame Chip Scale Package [LFCSP\_VD] 3 mm × 3 mm Body, Very Thin, Dual Lead (CP-8-2) Dimensions shown in millimeters

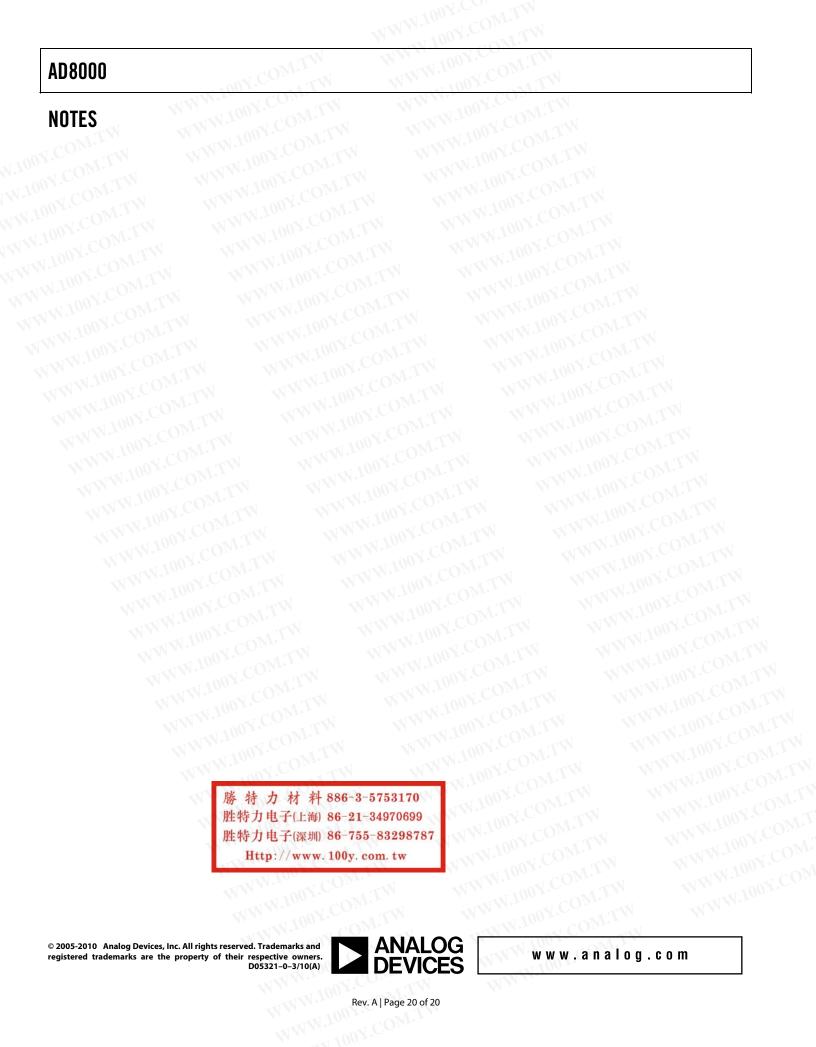
#### **ORDERING GUIDE**

Model <sup>1</sup>	Temperature Range	Package Description	Package Option	Branding	Ordering Quantity
AD8000YRDZ	-40°C to +125°C	8-Lead SOIC_N_EP	RD-8-1	A A A A A A A A A A A A A A A A A A A	Jun With
AD8000YRDZ-REEL	-40°C to +125°C	8-Lead SOIC_N_EP	RD-8-1	V.1 .	2,500
AD8000YRDZ-REEL7	-40°C to +125°C	8-Lead SOIC_N_EP	RD-8-1	MIL	1,000
AD8000YCPZ-R2	–40°C to +125°C	8-Lead LFCSP_VD	CP-8-2	HNB	250
AD8000YCPZ-REEL	-40°C to +125°C	8-Lead LFCSP_VD	CP-8-2	HNB	5,000
AD8000YCPZ-REEL7	-40°C to +125°C	8-Lead LFCSP_VD	CP-8-2	HNB	1,500



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