



# FSEZ1307 Primary-Side-Regulation PWM with Power MOSFET Integrated

#### **Features**

- Low Standby Power: Under 30mW
- High-Voltage Startup
- Few External Components
- Constant-Voltage (CV) and Constant-Current (CC)
   Control without Secondary-Feedback Circuitry
- Green Mode: Linearly Decreasing PWM Frequency
- Fixed PWM Frequency at 50kHz with Frequency Hopping to Solve EMI Problem
- Cable Compensation in CV Mode
- Peak-Current-Mode Control in CV Mode
- Cycle-by-Cycle Current Limiting
- V<sub>DD</sub> Over-Voltage Protection with Auto Restart
- V<sub>DD</sub> Under-Voltage Lockout (UVLO)
- Gate Output Maximum Voltage Clamped at 15V
- Fixed Over-Temperature Protection with Auto Restart
- Available in 7-Lead SOP Package

## **Applications**

- Battery chargers for cellular phones, cordless phones, PDA, digital cameras, power tools, etc.
- Replaces linear transformers and RCC SMPS

# Description

This third-generation Primary Side Regulation (PSR) PWM controller combination power MOSFET, FSEZ1307, provides several features to enhance the performance of low-power flyback converters. The proprietary topology, TRUECURRENT™, enables precise CC regulation and simplified circuit design for battery-charger applications. Compared to a conventional design or a linear transformer, a low-cost, smaller, and lighter charger results.

To minimize standby power consumption, the proprietary green mode provides off-time modulation to linearly decrease PWM frequency under light-load conditions. Green mode assists the power supply in meeting power conservation requirements.

By using the FSEZ1307, a charger can be implemented with few external components and minimized cost. A typical output CV/CC characteristic envelope is shown in Figure 1.

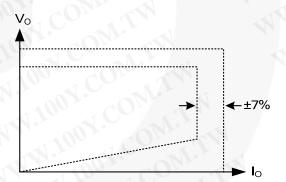


Figure 1. Typical Output V-I Characteristic

# **Ordering Information**

Part Number	Operating Temperature Range	© Eco Status	Package	Packing Method
FSEZ1307MY	-40°C to +105°C	Green 7-Lead, Small Outline Package (SOP-		Tape & Reel

Ø For Fairchild's definition of Eco Status, please visit: <a href="http://www.fairchildsemi.com/company/green/rohs\_green.html">http://www.fairchildsemi.com/company/green/rohs\_green.html</a>.

# **Application Diagram**

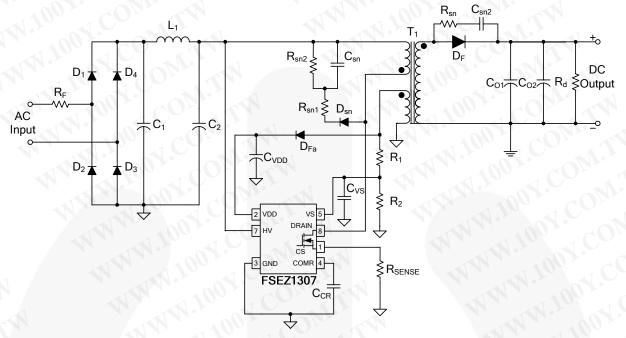
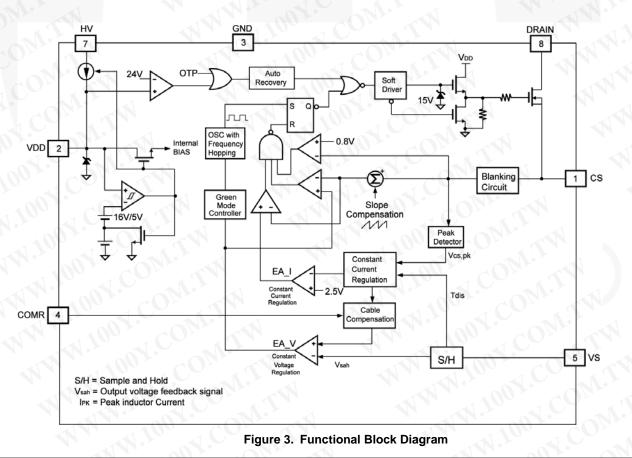


Figure 2. Typical Application

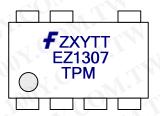
# **Internal Block Diagram**



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# **Marking Information**



- Fairchild Logo
- Z: Plant Code
- X: 1-Digit Year Code
  Y: 1-Digit Week Code
- TT: 2-Digit Die Run Code
- Package Type (M=SOP)
- P: Y=Green Package
- M: Manufacture Flow Code

Figure 4. Top Mark

# **Pin Configuration**

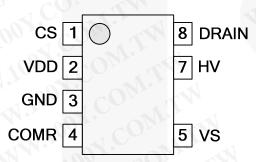


Figure 5. Pin Configuration

# **Pin Definitions**

Pin#	Name	Description
1	CS	Current Sense. This pin connects a current-sense resistor to detect the MOSFET current for peak-current-mode control in CV mode and provides the output-current regulation in CC mode.
2	VDD	<b>Power Supply</b> . IC operating current and MOSFET driving current are supplied using this pin. This pin is connected to an external V <sub>DD</sub> capacitor of typically 10μF. The threshold voltages for startup and turn-off are 16V and 5V, respectively. The operating current is lower than 5mA.
3	GND	Ground
4	COMR	<b>Cable Compensation</b> . This pin connects a 1µF capacitor between the COMR and GND pins for compensation voltage drop due to output cable loss in CV mode.
5	Vs	<b>Voltage Sense</b> . This pin detects the output voltage information and discharge time based on voltage of auxiliary winding.
7	HV	High Voltage. This pin connects to a bulk capacitor for high-voltage startup.
8	DRAIN	Driver Output. Power MOSFET drain. This pin is the high-voltage power MOSFET drain.

# **Absolute Maximum Ratings**

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Symbol		Min.	Max.	Units	
V <sub>HV</sub>	HV Pin Input Voltage	.1 (	500	V	
$V_{VDD}$	DC Supply Voltage <sup>(1,2)</sup>		107	30	V
V <sub>VS</sub>	VS Pin Input Voltage		-0.3	7.0	V
Vcs	CS Pin Input Voltage		-0.3	7.0	V
V <sub>COMV</sub>	Voltage Error Amplifier Outp	ut Voltage	-0.3	7.0	V
V <sub>СОМІ</sub>	Current Error Amplifier Outpo	ut Voltage	-0.3	7.0	V
V <sub>DS</sub>	Drain-Source Voltage	O. LA		700	V
1	Continuous Drain Current	T <sub>A</sub> =25°C		0.5	Α
Ι <sub>D</sub>	Continuous Drain Current	T <sub>A</sub> =100°C		0.35	1 A
I <sub>DM</sub>	Pulsed Drain Current		3.5	Α	
E <sub>AS</sub>	Single Pulse Avalanche Energy			35	mJ
I <sub>AR</sub>	Avalanche Current		1	Α	
P <sub>D</sub>	Power Dissipation (T <sub>A</sub> <50°C		660	mW	
heta JA	Thermal Resistance (Junctio	n to Air)		150	°C/W
heta JC	Thermal Resistance (Junctio	n to Case)		39	°C/W
TJ	Operating Junction Tempera	ture	-40	+150	°C
T <sub>STG</sub>	Storage Temperature Range			+150	°C
TL	Lead Temperature (Wave Soldering or IR, 10 Seconds)			+260	°C
ESD	Electrostatic Discharge	Human Body Model (Except HV Pin), JEDEC-JESD22_A114		2500	
ESD	Capability	Charged Device Model (Except HV Pin), JEDEC-JESD22_C101		1250	V

#### Notes:

- 1. Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device.
- 2. All voltage values, except differential voltages, are given with respect to the GND pin.

# **Recommended Operating Conditions**

The Recommended Operating Conditions table defines the conditions for actual device operation. Recommended operating conditions are specified to ensure optimal performance to the datasheet specifications. Fairchild does not recommend exceeding them or designing to Absolute Maximum Ratings.

Symbol	Parameter	Min.	Max.	Units
T <sub>A</sub>	Operating Ambient Temperature	-40	+105	°C

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# **Electrical Characteristics**

Unless otherwise specified, V<sub>DD</sub>=15V and T<sub>A</sub>=25°C.

Symbol	1. N	Parameter	Conditions	Min.	Тур.	Max.	Units
V <sub>DD</sub> Section	0		11/1/100		O is		
V <sub>OP</sub>	Continuously Oper	ating Voltage				23	V
$V_{DD-ON}$	Turn-On Threshold	Voltage	1	15	16	17	V
$V_{DD-OFF}$	Turn-Off Threshold	Voltage		4.5	5.0	5.5	V
I <sub>DD-OP</sub>	Operating Current				2.5	5.0	mA
I <sub>DD-GREEN</sub>	Green-Mode Opera	ating Supply Current		170	0.95	1.20	mA
V <sub>DD-OVP</sub>	V <sub>DD</sub> Over-Voltage-I	Protection Level (OVP)			24	40	V
V <sub>DD-OVP-HYS</sub>	Hysteresis Voltage	for V <sub>DD</sub> OVP		1.5	2.0	2.5	V
t <sub>D-VDDOVP</sub>	V <sub>DD</sub> Over-Voltage-Protection Debounce Time			50	200	300	μs
HV Startup (	Current Source Sec	tion		TO NOT	10	0 2.	40
$V_{HV-MIN}$	Minimum Startup V	oltage on HV Pin		<b>1</b>	11.7	50	V
I <sub>HV</sub>	Supply Current Dra	wn from HV Pin	V <sub>DC</sub> =100V	N	1.5	3.0	mA
I <sub>HV-LC</sub>	Leakage Current after Startup		HV=500V, V <sub>DD</sub> = V <sub>DD</sub> - <sub>OFF</sub> +1V	W	0.96	3.00	μА
Oscillator Se	ection			\<		×13	
	f Fraguenov	Center Frequency		47	50	53	101
fosc	Frequency	Frequency Hopping Range		±1.5	±2.0	±2.5	kHz
fosc-N-MIN	Minimum Frequence	cy at No-Load			370		Hz
f <sub>OSC-CM-MIN</sub>	Minimum Frequence	cy at CCM	Oh W		13		kHz
$f_{DV}$	Frequency Variation	n vs. V <sub>DD</sub> Deviation	V <sub>DD</sub> =10~25V,	<b>S</b> T	1	2	%
f <sub>DT</sub>	Frequency Variatio	n vs. Temperature Deviation	T <sub>A</sub> =-40°C to 105°C			15	%
Voltage-Sen	se Section		at Cork			4	
I <sub>tc</sub>	IC Bias Current		9, 40%		10		μA
V <sub>BIAS-COMV</sub>	Adaptive Bias Volta	age Dominated by V <sub>COMV</sub>	$R_{VS}=20k\Omega$		1.4		V
Current-Sen	se Section		(00)			7	4
t <sub>PD</sub>	Propagation Delay	to GATE Output	1003.	DIA.	90	200	ns
t <sub>MIN-N</sub>	Minimum On Time	at No-Load		700	850	1050	ns
V <sub>TH</sub>	Threshold Voltage	for Current Limit	1100	COR	0.8		V
Voltage-Erro	or-Amplifier Section		003				
$V_{VR}$	Reference Voltage			2.475	2.500	2.525	V
$V_N$	Green-Mode Starting Voltage on EA_V		f <sub>OSC</sub> -2kHz	10	2.5		V
$V_{G}$	Green-Mode Endin	g Voltage on EA_V	fosc=1kHz		0.4		V
Current-Erro	or-Amplifier Section					10	
V <sub>IR</sub>	Reference Voltage			2.475	2.500	2.525	V
Cable Comp	ensation Section	ON. AN			11.		
$V_{COMR}$	COMR Pin for Cab	le Compensation		111	0.75		V

Continued on the following page...

# **Electrical Characteristics** (Continued)

Unless otherwise specified, V<sub>DD</sub>=15V and T<sub>A</sub>=25°C.

Symbol	Parameter	Conditions	Min.	Тур.	Max.	Units
Internal MOS	SFET Section <sup>(3)</sup>	100		O.z.		
DCY <sub>MAX</sub>	Maximum Duty Cycle		70	75	80	%
$BV_{DSS}$	Drain-Source Breakdown Voltage	I <sub>D</sub> =250μA, V <sub>GS</sub> =0V	700	Co		V
ΔBV <sub>DSS</sub> /ΔT <sub>J</sub> Breakdown Voltage Temperature Coefficient		I <sub>D</sub> =250µA, Referenced to T <sub>A</sub> =25°C	N.100	0.53	-0 <sup>1</sup> / <sub>2</sub>	V/°C
R <sub>DS(ON)</sub>	Static Drain-Source On-Resistance	I <sub>D</sub> =0.5A, V <sub>GS</sub> =10V		17	20	Ω
Is	Maximum Continuous Drain-Source Diode Forward Current		NY	.100	0.5	A
.1	DAMA TOO COM THE	V <sub>DS</sub> =700V, T <sub>A</sub> =25°C	NN	N	10	μА
I <sub>DSS</sub>	Drain-Source Leakage Current	V <sub>DS</sub> =560V, T <sub>A</sub> =100°C			100	μА
t <sub>D-ON</sub>	Turn-On Delay Time	V <sub>DS</sub> =350V,	\<	10	30	ns
t <sub>D-OFF</sub>	Turn-Off Delay Time	$I_D=1A$ , $R_G=25\Omega^{(4)}$		20	50	ns
C <sub>ISS</sub> Input Capacitance		$V_{GS}$ =0V, $V_{DS}$ =25V, $f_{S}$ =1MHz		125	150	pF
Coss Output Capacitance			N	15	18	pF
Over-Tempe	rature-Protection Section		-1			
T <sub>OTP</sub>	Threshold Temperature for OTP <sup>(5)</sup>	COR		140		°C

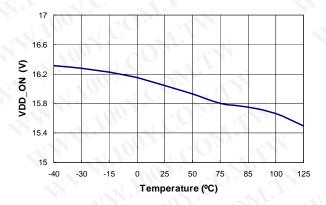
#### Notes:

- 3. These parameters, although guaranteed, are not 100% tested in production.
- 4. Pulse test: pulsewidth  $\leq 300 \mu s$ , duty cycle  $\leq 2\%$ .
- 5. When the Over-temperature protection is activated, the power system enter latch mode and output is disabled.

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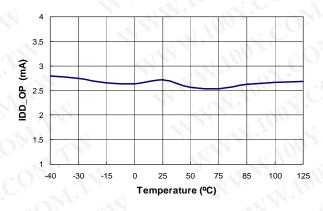
# **Typical Performance Characteristics**



5.5 5.3 5.1 5.1 4.7 4.5 -40 -30 -15 0 25 50 75 85 100 125 Temperature (°C)

Figure 6. Turn-On Threshold Voltage (V<sub>DD-ON</sub>) vs. Temperature

Figure 7. Turn-Off Threshold Voltage (V<sub>DD-OFF</sub>) vs. Temperature



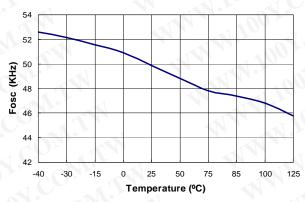
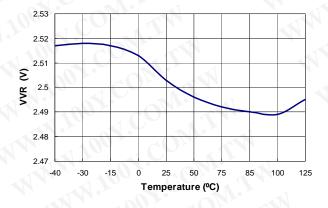


Figure 8. Operating Current (I<sub>DD-OP</sub>) vs. Temperature

Figure 9. Center Frequency (fosc) vs. Temperature



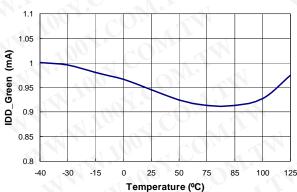
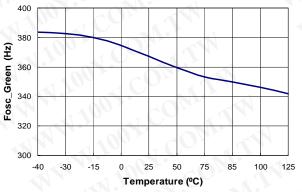


Figure 10. Reference Voltage (V<sub>VR</sub>) vs. Temperature

Figure 11. Green-Mode Operating Supply Current (I<sub>DD-GREEN</sub>) vs. Temperature

# **Typical Performance Characteristics**



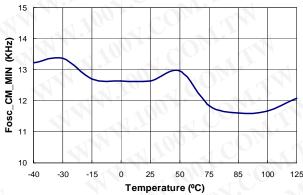
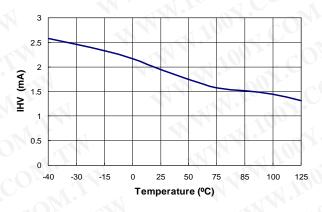


Figure 12. Minimum Frequency at No Load (fosc-N-MIN) vs. Temperature

Figure 13. Minimum Frequency at CCM (f<sub>OSC-CM-MIN</sub>) vs. Temperature



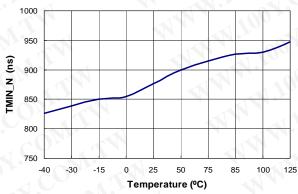
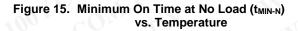
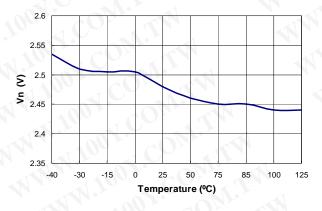


Figure 14. Supply Current Drawn from HV Pin (I<sub>HV</sub>) vs. Temperature





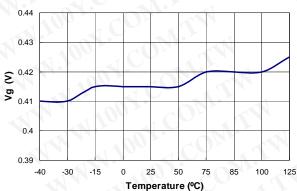
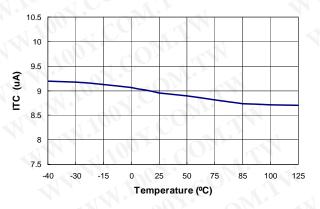


Figure 16. Green-Mode Starting Voltage on EA\_V  $(V_N)$  vs. Temperature

Figure 17. Green-Mode Ending Voltage on EA\_V (V<sub>G</sub>) vs. Temperature

# **Typical Performance Characteristics**



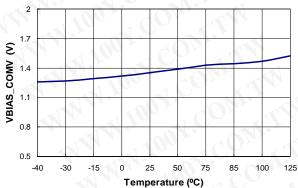
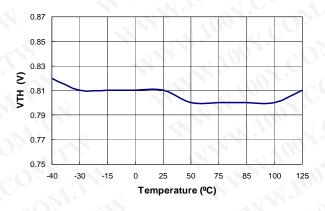


Figure 18. IC Bias Current (Itc) vs. Temperature

Figure 19. Adaptive Bias Voltage Dominated by V<sub>COMV</sub> (V<sub>BIAS-COMV</sub>) vs. Temperature



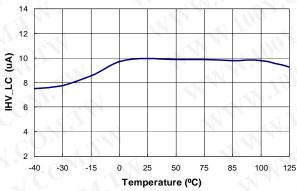
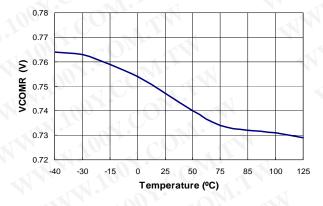


Figure 20. Threshold Voltage for Current Limit (V<sub>TH</sub>) vs. Temperature

Figure 21. Leakage Current after Startup (I<sub>HV-LC</sub>) vs. Temperature



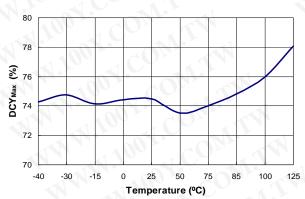


Figure 22. Variation Test Voltage on COMR Pin for Cable Compensation ( $V_{\text{COMR}}$ ) vs. Temperature

Figure 23. Maximum Duty Cycle (DCY<sub>MAX</sub>) vs. Temperature

# **Functional Description**

Figure 24 shows the basic circuit diagram of primary-side regulated flyback converter, with typical waveforms shown in Figure 25. Generally, discontinuous conduction mode (DCM) operation is preferred for primary-side regulation because it allows better output regulation. The operation principles of DCM flyback converter are as follows:

During the MOSFET on time ( $t_{ON}$ ), input voltage ( $V_{DL}$ ) is applied across the primary-side inductor ( $L_m$ ). Then MOSFET current ( $I_{ds}$ ) increases linearly from zero to the peak value ( $I_{pk}$ ). During this time, the energy is drawn from the input and stored in the inductor.

When the MOSFET is turned off, the energy stored in the inductor forces the rectifier diode (D) to be turned on. While the diode is conducting, the output voltage  $(V_0)$ , together with diode forward-voltage drop  $(V_F)$ , is applied across the secondary-side inductor  $(L_m \times N_s^2/N_\rho^2)$  and the diode current  $(I_D)$  decreases linearly from the peak value  $(I_{pk} \times N_p/N_s)$  to zero. At the end of inductor current discharge time  $(t_{DIS})$ , all the energy stored in the inductor has been delivered to the output.

When the diode current reaches zero, the transformer auxiliary winding voltage  $(V_w)$  begins to oscillate by the resonance between the primary-side inductor  $(L_m)$  and the effective capacitor loaded across the MOSFET.

During the inductor current discharge time, the sum of output voltage and diode forward-voltage drop is reflected to the auxiliary winding side as  $(V_o+V_F) \times N_a/N_s$ . Since the diode forward-voltage drop decreases as current decreases, the auxiliary winding voltage reflects the output voltage best at the end of diode conduction time where the diode current diminishes to zero. Thus, by sampling the winding voltage at the end of the diode conduction time, the output voltage information can be obtained. The internal error amplifier for output voltage regulation (EA\_V) compares the sampled voltage with internal precise reference to generate error voltage ( $V_{COMV}$ ), which determines the duty cycle of the MOSFET in CV mode.

Meanwhile, the output current can be estimated using the peak drain current and inductor current discharge time because output current is same as the average of the diode current in steady state.

The output current estimator picks up the peak value of the drain current with a peak detection circuit and calculates the output current using the inductor discharge time  $(t_{\text{DIS}})$  and switching period  $(t_{\text{s}})$ . This output information is compared with internal precise reference to generate the error voltage  $(V_{\text{COMI}})$ , which determines the duty cycle of the MOSFET in CC mode. With Fairchild's innovative TRUECURRENTTM technique, constant current (CC) output can be precisely controlled.

Among the two error voltages,  $V_{\text{COMV}}$  and  $V_{\text{COMI}}$ , the smaller one determines the duty cycle. Therefore, during constant voltage regulation mode,  $V_{\text{COMV}}$  determines the

duty cycle while  $V_{\text{COMI}}$  is saturated to HIGH. During constant current regulation mode,  $V_{\text{COMI}}$  determines the duty cycle while  $V_{\text{COMV}}$  is saturated to HIGH.

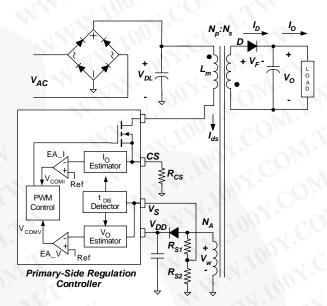


Figure 24. Simplified PSR Flyback Converter Circuit

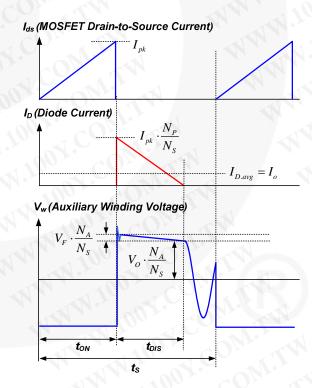


Figure 25. Key Waveforms of DCM Flyback Converter

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# **Cable Voltage Drop Compensation**

In cellular phone charger applications, the battery is located at the end of cable, which typically causes several percentage points of voltage drop on the battery voltage. FSEZ1307 has a built-in cable voltage drop compensation that provides a constant output voltage at the end of the cable over the entire load range in CV mode. As load increases, the voltage drop across the cable is compensated by increasing the reference voltage of the voltage regulation error amplifier.

## **Operating Current**

The FSEZ1307 operating current is as small as 2.5mA, which results in higher efficiency and reduces the  $V_{DD}$  hold-up capacitance requirement. Once FSEZ1307 enters "deep" green mode, the operating current is reduced to 0.95mA, assisting the power supply in meeting power conservation requirements.

## **Green-Mode Operation**

The FSEZ1307 uses voltage regulation error amplifier output ( $V_{\text{COMV}}$ ) as an indicator of the output load and modulates the PWM frequency, as shown in Figure 26. The switching frequency decreases as the load decreases. In heavy load conditions, the switching frequency is fixed at 50kHz. Once  $V_{\text{COMV}}$  decreases below 2.5V, the PWM frequency linearly decreases from 50kHz. When FSEZ1307 enters deep green mode, the PWM frequency is reduced to a minimum frequency of 370Hz, gaining power saving to meet international power conservation requirements.

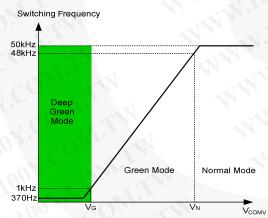


Figure 26. Switching Frequency in Green Mode

## Frequency Hopping

EMI reduction is accomplished by frequency hopping, which spreads the energy over a wider frequency range than the bandwidth measured by the EMI test equipment. FSEZ1307 has an internal frequency hopping circuit that changes the switching frequency between 47kHz and 53kHz over the period shown in Figure 27.

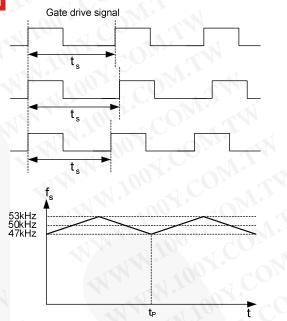


Figure 27. Frequency Hopping

## **High-Voltage Startup**

Figure 28 shows the HV-startup circuit for FSEZ1307 applications. The HV pin is connected to the line input or bulk capacitor through a resistor,  $R_{\rm START}$  (100k $\Omega$  recommended). During startup, the internal startup circuit is enabled. Meanwhile, line input supplies the current,  $I_{\rm STARTUP}$ , to charge the hold-up capacitor,  $C_{\rm DD}$ , through  $R_{\rm START}$ . When the  $V_{\rm DD}$  voltage reaches  $V_{\rm DD-ON}$ , the internal startup circuit is disabled, blocking  $I_{\rm STARTUP}$  from flowing into the HV pin. Once the IC turns on,  $C_{\rm DD}$  is the only energy source to supply the IC consumption current before the PWM starts to switch. Therefore,  $C_{\rm DD}$  must be large enough to prevent  $V_{\rm DD}$  from dropping down to  $V_{\rm DD-OFF}$  before the power can be delivered from the auxiliary winding.

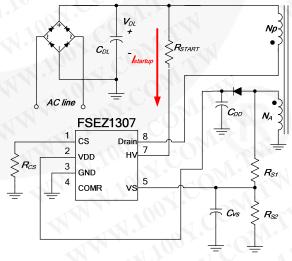


Figure 28. HV Startup Circuit

## **Under-Voltage Lockout (UVLO)**

The turn-on and turn-off thresholds are fixed internally at 16V and 5V, respectively. During startup, the hold-up capacitor must be charged to 16V through the startup resistor to enable the FSEZ1307. The hold-up capacitor continues to supply  $V_{\text{DD}}$  until power can be delivered from the auxiliary winding of the main transformer.  $V_{\text{DD}}$  is not allowed to drop below 5V during this startup process. This UVLO hysteresis window ensures that hold-up capacitor properly supplies  $V_{\text{DD}}$  during startup.

#### **Protections**

The FSEZ1307 has several self-protection functions, such as Over-Voltage Protection (OVP), Over-Temperature Protection (OTP), and pulse-by-pulse current limit. All the protections are implemented as auto-restart mode. Once the abnormal condition occurs, the switching is terminated and the MOSFET remains off, causing  $V_{DD}$  to drop. When  $V_{DD}$  drops to the  $V_{DD}$  turn-off voltage of 5V, the internal startup circuit is enabled again and the supply current drawn from the HV pin charges the hold-up capacitor. When  $V_{DD}$  reaches the turn-on voltage of 16V, normal operation resumes. In this manner, the auto-restart alternately enables and disables the switching of the MOSFET until the abnormal condition is eliminated (see Figure 29).

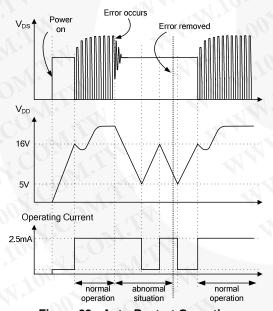


Figure 29. Auto-Restart Operation

### **V<sub>DD</sub> Over-Voltage Protection (OVP)**

 $V_{DD}$  over-voltage protection prevents damage from over-voltage conditions. If the  $V_{DD}$  voltage exceeds 24V at open-loop feedback condition, OVP is triggered and the PWM switching is disabled. The OVP has a debounce time (typically 200 $\mu s$ ) to prevent false triggering due to switching noises.

## **Over-Temperature Protection (OTP)**

The built-in temperature-sensing circuit shuts down PWM output if the junction temperature exceeds 140°C.

#### **Pulse-by-Pulse Current Limit**

When the sensing voltage across the current-sense resistor exceeds the internal threshold of 0.8V, the MOSFET is turned off for the remainder of switching cycle. In normal operation, the pulse-by-pulse current limit is not triggered since the peak current is limited by the control loop.

## Leading-Edge Blanking (LEB)

Each time the power MOSFET switches on, a turn-on spike occurs at the sense resistor. To avoid premature termination of the switching pulse, a leading-edge blanking time is built in. During this blanking period, the current-limit comparator is disabled and cannot switch off the gate driver. As a result, conventional RC filtering can be omitted.

## **Gate Output**

The FSEZ1307 output stage is a fast totem-pole gate driver. Cross conduction has been avoided to minimize heat dissipation, increase efficiency, and enhance reliability. The output driver is clamped by an internal 15V Zener diode to protect the power MOSFET transistors against undesired over-voltage gate signals.

## **Built-In Slope Compensation**

The sensed voltage across the current-sense resistor is used for current mode control and pulse-by-pulse current limiting. Built-in slope compensation improves stability and prevents sub-harmonic oscillations due to peak-current mode control. The FSEZ1307 has a synchronized, positive-slope ramp built-in at each switching cycle.

#### **Noise Immunity**

Noise from the current sense or the control signal can cause significant pulsewidth jitter, particularly in continuous-conduction mode. While slope compensation helps alleviate these problems, further precautions should still be taken. Good placement and layout practices should be followed. Avoiding long PCB traces and component leads, locating compensation and filter components near the FSEZ1307, and increasing the power MOS gate resistance are advised.

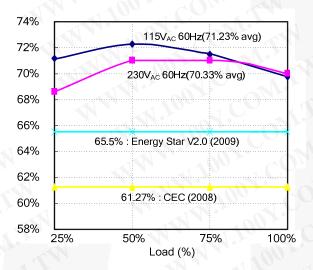
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# Typical Application Circuit (Primary-Side Regulated Flyback Charger)

Application	Fairchild Device	Input Voltage Range	Output	Output DC cable
Cell Phone Charger	FSEZ1307	90~265V <sub>AC</sub>	5V/0.7A (3.5W)	AWG26, 1.8 Meter

#### **Features**

- High efficiency (>65.5% at full load) meeting EPS 2.0 regulation with enough margin
- Low standby (Pin<30mW at no-load condition)



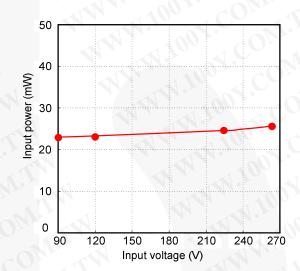


Figure 30. Measured Efficiency

Figure 31. Standby Power

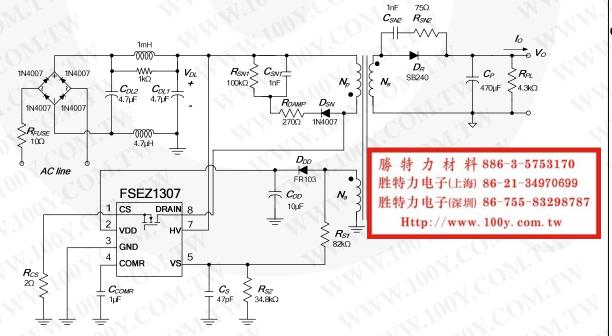


Figure 32. Schematic of Typical Application Circuit

# **Typical Application Circuit (Continued)**

# **Transformer Specification**

Core: EE16Bobbin: EE16

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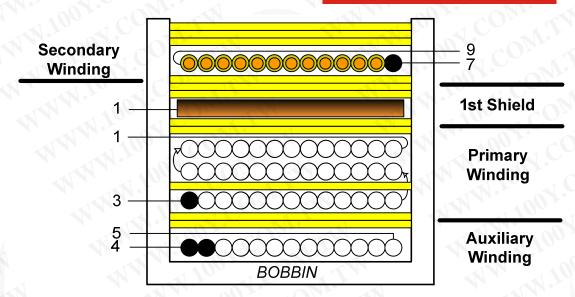


Figure 33. Transformer Specification

#### Notes:

- 6. When W4R's winding is reversed winding, it must wind one layer.
- 7. When W2 is winding, it must wind three layers and put one layer of tape after winding the first layer.

TERMI	TERMINAL			INSULATION	BARRIER TAPE		
NO	S	F	WIRE	t <sub>s</sub>	t <sub>s</sub>	Primary	Seconds
W1	4	5	2UEW 0.23*2	15	2		1/41
	O.			41	1		
W2	3	1	2UEW 0.17*1	39	0		
00				37	2		
W3	1.	No.	COPPER SHIELD	1.2	3		
W4	7	9	TEX-E 0.55*1	9	3		1
110		O >	CORE ROUNDING TAPE		3		

M. M. Ing Co.	Pin	Specification	Remark
Primary-Side Inductance	1-3	2.25mH ± 7%	100kHz, 1V
Primary-Side Effective Leakage	1-3	80μH ± 5%	Short One of the Secondary Windings

### 胜特力电子(深圳) 86-755-83298787 **Physical Dimensions** Http://www. 100y. com. tw 5.00 4.80 Α 0.65 3.81 8 В 6.20 4.00 5.60 5.80 3.80 PIN ONE **INDICATOR** 1.27 (0.33)⊕ 0.25 M C B A LAND PATTERN RECOMMENDATION SEE DETAIL A 0.25 0.10 0.25 1.75 MAX 0.19 ○ 0.10 C 0.51 **OPTION A - BEVEL EDGE** 0.33 0.50 x 45° 0.25 R<sub>0.10</sub> **GAGE PLANE** OPTION B - NO BEVEL EDGE R<sub>0.10</sub> 0.36 NOTES: 8° A) THIS PACKAGE CONFORMS TO JEDEC O° MS-012 VARIATION AA EXCEPT FOR MISSING PIN 6. B) ALL DIMENSIONS ARE IN MILLIMETERS. 0.90 SEATING PLANE C) DIMENSIONS DO NOT INCLUDE MOLD 0.406 (1.04)FLASH OR BURRS. D) DRAWING FILENAME: M07BREV2 **DETAIL A**

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Figure 34. 7-Lead, Small Outline Package (SOP-7)

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