

Data Sheet August 2001 File Number 1050.5

# Dual, 4.5MHz, BiMOS Operational Amplifier with MOSFET Input/Bipolar Output

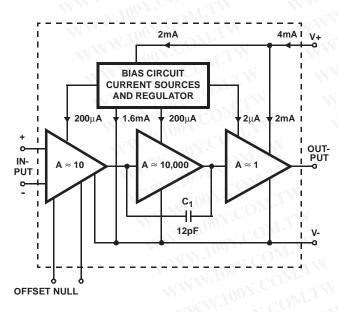
The CA3240A and CA3240 are dual versions of the popular CA3140 series integrated circuit operational amplifiers. They combine the advantages of MOS and bipolar transistors on the same monolithic chip. The gate-protected MOSFET (PMOS) input transistors provide high input impedance and a wide common-mode input voltage range (typically to 0.5V below the negative supply rail). The bipolar output transistors allow a wide output voltage swing and provide a high output current capability.

The CA3240A and CA3240 are compatible with the industry standard 1458 operational amplifiers in similar packages. The offset null feature is available only when these types are supplied in the 14 lead PDIP package (E1 suffix).

## **Ordering Information**

PART NUMBER	TEMP. RANGE (°C)	PACKAGE	PKG. NO.
CA3240AE	-40 to 85	8 Ld PDIP	E8.3
CA3240AE1	-40 to 85	14 Ld PDIP	E14.3
CA3240E	-40 to 85	8 Ld PDIP	E8.3

# Functional Diagram



NOTE: Only available with 14 lead DIP (E1 Suffix)

#### **Features**

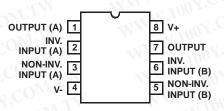
- Dual Version of CA3140
- · Internally Compensated
- MOSFET Input Stage
  - Very High Input Impedance ( $Z_{IN}$ ) 1.5T $\Omega$  (Typ)
  - Very Low Input Current (II) 10pA (Typ) at ±15V
  - Wide Common-Mode Input Voltage Range ( $V_{ICR}$ ): Can Be Swung 0.5V Below Negative Supply Voltage Rail
- Directly Replaces Industry Type 741 in Most Applications

## **Applications**

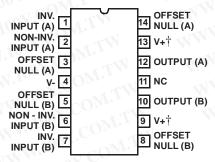
- Ground Referenced Single Amplifiers in Automobile and Portable Instrumentation
- Sample and Hold Amplifiers
- Long Duration Timers/Multivibrators (Microseconds-Minutes-Hours)
- Photocurrent Instrumentation
- Intrusion Alarm System
- Active Filters
- Comparators
- Function Generators
- Instrumentation Amplifiers
- Power Supplies

## **Pinouts**





#### CA3240A (PDIP) TOP VIEW



 $\dagger$  Pins 9 and 13 internally connected through approximately 3 $\Omega$ .

#### **Absolute Maximum Ratings**

Supply Voltage (Between V+ and V-)	36V
Differential Input Voltage	8V
Input Voltage (V+ +8V) to (V0	.5V)
Input Current	ImA
Output Short Circuit Duration (Note 1) Indef	inite

# Thermal Information

Thermal Resistance (Typical, Note 2)	$\theta_{JA}$ (oC/W)
8 Lead PDIP Package	100
14 Lead PDIP Package	
Maximum Junction Temperature (Plastic Package)	150°C
Maximum Storage Temperature Range65	<sup>o</sup> C to 150 <sup>o</sup> C
Maximum Lead Temperature (Soldering 10s)	300°C

#### Operating Conditions

Temperature Range		1.09	-40°C to 85°C
Voltage Range	J. W. N. I.	4V to 36V	or ±2V to ±18V

CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.

#### NOTES

- 1. Short circuit may be applied to ground or to either supply. Temperatures and/or supply voltages must be limited to keep dissipation within maximum rating.
- 2.  $\theta_{JA}$  is measured with the component mounted on an evaluation PC board in free air.

## **Electrical Specifications** For Equipment Design, $V_{SUPPLY} = \pm 15V$ , $T_A = 25^{\circ}C$ , Unless Otherwise Specified

TINOY.COMITY	MA	CA3240			W	CA3240A	Vii	
PARAMETER	SYMBOL	MIN	TYP	MAX	MIN	TYP	MAX	UNITS
Input Offset Voltage	V <sub>IO</sub>	NW:	C 5	15	M-M.	2	5	mV
Input Offset Current	I <sub>IO</sub>	11/1/10	0.5	30	TWI	0.5	20	pA
Input Current	I <sub>I</sub>	TIN.1	10	50	- 30	10	40	pА
Large-Signal Voltage Gain	A <sub>OL</sub>	20	100	W.T.W	20	100	TIVOD	kV/V
(See Figures 13, 28) (Note 3)	N	86	100	FW	86	100	.Co-	dB
Common Mode Rejection CMRF Ratio (See Figure 18)	CMRR	-xi-WV	32	320	- 🕠	32	320	μV/V
		70	90	OW	70	90	~ COM	dB
Common Mode Input Voltage Range (See Figure 25)	V <sub>ICR</sub>	-15	-15.5 to +12.5	CO11.	-15	-15.5 to +12.5	12	V
Power Supply Rejection Ratio	PSRR	-	100	150		100	150	μV/V
(See Figure 20)	$(\Delta V_{IO}/\Delta V\pm)$	76	80	Moo	76	80	700 - C	dB
Maximum Output Voltage (Note 4)	V <sub>OM</sub> +	12	13	14.6	12	13	1700x.	V
(See Figures 24, 25)	V <sub>OM</sub> -	-14	-14.4	WY.CO.	-14	-14.4	1007.	V
Maximum Output Voltage (Note 5)	V <sub>OM</sub> -	0.4	0.13	-CO	0.4	0.13	You.	V
Total Supply Current (See Figure 16) For Both Amps	CO1+1.1	W -	8	12 C	MITW	8	12	mA
Total Device Dissipation	CP <sub>D</sub>	rW-	240	360	WITE	240	360	mW

#### NOTES:

- 3. At  $V_O = 26V_{P-P}$ , +12V, -14V and  $R_L = 2k\Omega$ .
- 4. At  $R_L = 2k\Omega$ .
- 5. At V+ = 5V, V- = GND,  $I_{SINK}$  = 200 $\mu$ A.

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## **Electrical Specifications** For Equipment Design, $V_{SUPPLY} = \pm 15V$ , $T_A = 25^{\circ}C$ , Unless Otherwise Specified

1/1/1/1003	I.C.	IN W. W. 1001.	TYPICAL	VALUES	100 7
PARAMETER	SYMBOL	TEST CONDITIONS	CA3240A	CA3240	UNITS
Input Offset Voltage Adjustment Resistor (E1 Package Only)	OY.COD	Typical Value of Resistor Between Terminals 4 and 3(5) or Between 4 and 14(8) to Adjust Maximum V <sub>IO</sub>	18	4.7	kΩ
Input Resistance	$R_{I}$	MITH WWW. TILOUT. COM	1.5	1.5	ΤΩ
Input Capacitance	C <sub>I</sub> C	WWW. 100X.CO	4	4	pF
Output Resistance	R <sub>O</sub>	OM. COM	60	60	Ω
Equivalent Wideband Input Noise Voltage (See Figure 2)	e <sub>N</sub>	BW = 140kHz, $R_S = 1M\Omega$	48	48	μV

## **Electrical Specifications** For Equipment Design, $V_{SUPPLY} = \pm 15V$ , $T_A = 25^{\circ}C$ , Unless Otherwise Specified (Continued)

WWW. TOOX.Co	TW	MM	WILL	TYPICAL	VALUES	
PARAMETER	SYMBOL	TEST CONDITION	IS	CA3240A	CA3240	UNITS
Equivalent Input Noise Voltage	e <sub>N</sub>	$f = 1kHz, R_S = 100\Omega$	COM	40	40	nV/√Hz
(See Figure 19)	TIMOS	$f = 10kHz, R_S = 100\Omega$		12	12	nV/√Hz
Short-Circuit Current to Opposite Supply	I <sub>OM</sub> +	Source	. ON TW	40	40	mA
	I <sub>OM</sub> -	Sink		11	11	mA
Gain Bandwidth Product (See Figures 14, 28)	f <sub>T</sub>	WWW.	ON.COM	4.5	4.5	MHz
Slew Rate (See Figure 15)	SR	A. W.W.M	COM.	9	9	V/μs
Transient Response (See Figure 1)	00 t <sub>r</sub>	$R_L = 2k\Omega$ , $C_L = 100pF$	Rise Time	0.08	0.08	μs
	OS	$R_L = 2k\Omega$ , $C_L = 100pF$	Overshoot	10	10	%
Settling Time at 10V <sub>P-P</sub> (See Figure 26)	ts	$A_V = +1, R_L = 2k\Omega, C_L = 100pF,$	To 1mV	4.5	4.5	μs
	1.100	Voltage Follower	To 10mV	1.4	1.4	μs
Crosstalk (See Figure 23)	N.100 r.	f = 1kHz	11.100 C	120	120	dB

## **Electrical Specifications** For Equipment Design, at $V_{SUPPLY} = \pm 15V$ , $T_A = -40$ to $85^{\circ}$ C, Unless Otherwise Specified

IN TOO E COM. THE STANK TH	ON	TYPICAL		
PARAMETER	SYMBOL	CA3240A	CA3240	UNITS
Input Offset Voltage	IVIOI	3	10	mV
Input Offset Current (Note 8)	liol	32	32	pA
Input Current (Note 8)	I CO III	640	640	pA
Large Signal Voltage Gain (See Figures 13, 28), (Note 6)	AoL	63	63	kV/V
	$O_{M'I}$	96	96	dB
Common Mode Rejection Ratio (See Figure 18)	CMRR	32	32	μV/V
		90	90	dB
Common Mode Input Voltage Range (See Figure 25)	V <sub>ICR</sub>	-15 to +12.3	-15 to +12.3	V
Power Supply Rejection Ratio (See Figure 20)	PSRR	150	150	μV/V
	$(\Delta V_{IO}/\Delta V\pm)$	76	76	dB
Maximum Output Voltage (Note 7) (See Figures 24, 25)	V <sub>OM</sub> +	12.4	12.4	V
	V <sub>OM</sub> -	-14.2	-14.2	V
Supply Current (See Figure 16) Total For Both Amps	VIVI Ity CC	8.4	8.4	mA
Total Device Dissipation	PD	252	252	mW
Temperature Coefficient of Input Offset Voltage	$\Delta V_{IO}/\Delta T$	15	15	μV/ <sup>o</sup> C

#### NOTES:

- 6. At  $V_O$  = 26V<sub>P-P</sub>, +12V, -14V and  $R_L$  =  $2k\Omega.$
- 7. At  $R_L = 2k\Omega$ .
- 8. At  $T_A = 85^{\circ}C$ .

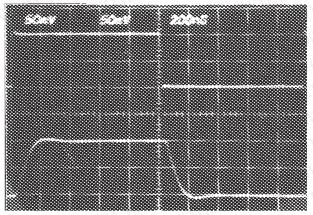
## **Electrical Specifications** For Equipment Design, at V+ = 5V, V- = 0V, T<sub>A</sub> = 25°C, Unless Otherwise Specified

M. 100 COW. T.	L.WW.	TYPICA	W.Iv	
PARAMETER	SYMBOL	CA3240A	CA3240	UNITS
Input Offset Voltage	V <sub>IO</sub>	100 2	5	mV
Input Offset Current	liol	0.1	0.1	рА
Input Current	I I WIN	2, CO	2	pA
Input Resistance	R <sub>IN</sub>	W.101	1	ΤΩ
Large Signal Voltage Gain (See Figures 13, 28)	A <sub>OL</sub>	100	100	kV/V
	W W	100	100	dB

**Electrical Specifications** For Equipment Design, at V+ = 5V, V- = 0V,  $T_A = 25^{\circ}C$ , Unless Otherwise Specified (Continued)

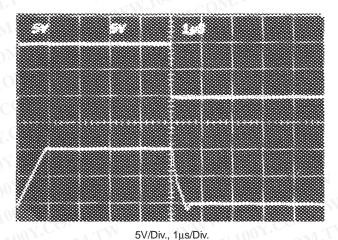
PARAMETER		100	TYPICAL VALUES			
		SYMBOL	CA3240A	CA3240	UNITS	
Common-Mode Rejection Ratio		CMRR	32	32	μV/V	
		W.1	90	90	dB	
Common-Mode Input Voltage Range (See Figure 25	5) (1)	V <sub>ICR</sub>	-0.5	-0.5	V	
		MMW.	2.6	2.6	V	
Power Supply Rejection Ratio		PSRR	31.6	31.6	μV/V	
			90	90	dB	
Maximum Output Voltage (See Figures 24, 25)	TIME	V <sub>OM</sub> +	10/3	3	V	
		V <sub>OM</sub> -	0.3	0.3	V	
Maximum Output Current	Source	I <sub>OM</sub> +	20	20	mA	
	Sink	I <sub>OM</sub> -	TOWN IT	1	mA	
Slew Rate (See Figure 15)		SR	7,00	7	V/µs	
Gain Bandwidth Product (See Figure 14)		f <sub>T</sub>	4.5	4.5	MHz	
Supply Current (See Figure 16)		I+	4	4	mA	
Device Dissipation	1.100 COL	P <sub>D</sub>	20	20	mW	

## **Test Circuits and Waveforms**



50mV/Div., 200ns/Div. Top Trace: Input, Bottom Trace: Output

FIGURE 1A. SMALL SIGNAL RESPONSE



Top Trace: Input, Bottom Trace: Output

FIGURE 1B. LARGE SIGNAL RESPONSE

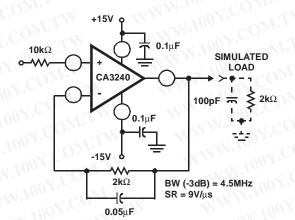


FIGURE 1C. TEST CIRCUIT

FIGURE 1. SPLIT-SUPPLY VOLTAGE FOLLOWER TEST CIRCUIT AND ASSOCIATED WAVEFORMS

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## Test Circuits and Waveforms (Continued)

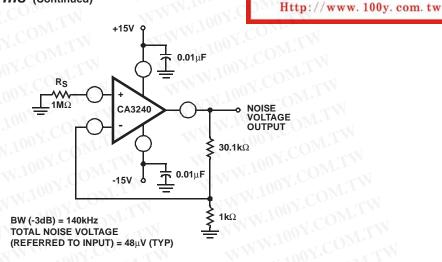
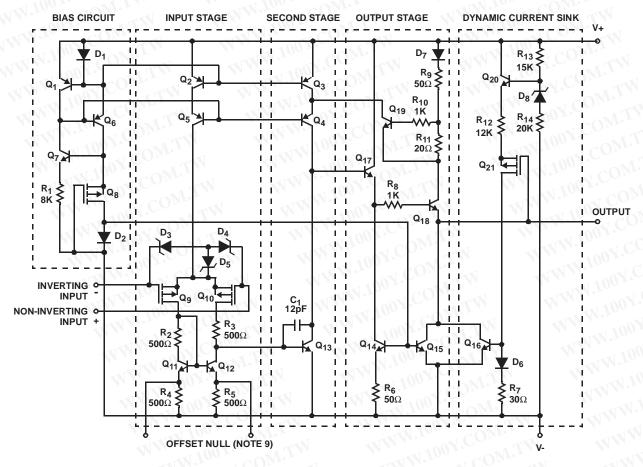


FIGURE 2. TEST CIRCUIT AMPLIFIER (30dB GAIN) USED FOR WIDEBAND NOISE MEASUREMENT

#### **Schematic Diagram** (One Amplifier of Two)



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#### NOTES:

- 9. Only available with 14 Lead DIP (E1 Suffix).
- 10. All resistance values are in ohms.

## Application Information

#### Circuit Description

The schematic diagram details one amplifier section of the CA3240. It consists of a differential amplifier stage using PMOS transistors ( $Q_9$  and  $Q_{10}$ ) with gate-to-source protection against static discharge damage provided by zener diodes  $D_3$ ,  $D_4$ , and  $D_5$ . Constant current bias is applied to the differential amplifier from transistors  $Q_2$  and  $Q_5$  connected as a constant current source. This assures a high common-mode rejection ratio. The output of the differential amplifier is coupled to the base of gain stage transistor  $Q_{13}$  by means of an NPN current mirror that supplies the required differential-to-single-ended conversion. Provision for offset null for types in the 14 lead plastic package (E1 suffix) is provided through the use of this current mirror.

The gain stage transistor Q<sub>13</sub> has a high impedance active load (Q3 and Q4) to provide maximum open-loop gain. The collector of Q<sub>13</sub> directly drives the base of the compound emitter-follower output stage. Pulldown for the output stage is provided by two independent circuits: (1) constant-currentconnected transistors Q<sub>14</sub> and Q<sub>15</sub> and (2) dynamic currentsink transistor Q<sub>16</sub> and its associated circuitry. The level of pulldown current is constant at about 1mA for Q<sub>15</sub> and varies from 0 to 18mA for Q<sub>16</sub> depending on the magnitude of the voltage between the output terminal and V+. The dynamic current sink becomes active whenever the output terminal is more negative than V+ by about 15V. When this condition exists, transistors Q<sub>21</sub> and Q<sub>16</sub> are turned on causing Q<sub>16</sub> to sink current from the output terminal to V-. This current always flows when the output is in the linear region, either from the load resistor or from the emitter of Q<sub>18</sub> if no load resistor is present. The purpose of this dynamic sink is to permit the output to go within 0.2V ( $V_{CE}$  (sat)) of V- with a  $2k\Omega$  load to ground. When the load is returned to V+, it may be necessary to supplement the 1mA of current from Q<sub>15</sub> in order to turn on the dynamic current sink (Q<sub>16</sub>). This may be accomplished by placing a resistor (Approx.  $2k\Omega$ ) between the output and V-.

## **Output Circuit Considerations**

Figure 24 shows output current-sinking capabilities of the CA3240 at various supply voltages. Output voltage swing to the negative supply rail permits this device to operate both power transistors and thyristors directly without the need for level-shifting circuitry usually associated with the 741 series of operational amplifiers.

Figure 3 shows some typical configurations. Note that a series resistor, RL, is used in both cases to limit the drive available to the driven device. Moreover, it is recommended that a series diode and shunt diode be used at the thyristor input to prevent large negative transient surges that can appear at the gate of thyristors, from damaging the integrated circuit.

#### Input Circuit Considerations

As indicated by the typical VICR, this device will accept inputs as low as 0.5V below V-. However, a series current-limiting resistor is recommended to limit the maximum input terminal current to less than 1mA to prevent damage to the input protection circuitry.

Moreover, some current-limiting resistance should be provided between the inverting input and the output when the CA3240 is used as a unity-gain voltage follower. This resistance prevents the possibility of extremely large input-signal transients from forcing a signal through the input-protection network and directly driving the internal constant-current source which could result in positive feedback via the output terminal. A  $3.9 \mathrm{k}\Omega$  resistor is sufficient.

The typical input current is on the order of 10pA when the inputs are centered at nominal device dissipation. As the output supplies load current, device dissipation will increase, rasing the chip temperature and resulting in increased input current. Figure 4 shows typical input-terminal current versus ambient temperature for the CA3240.

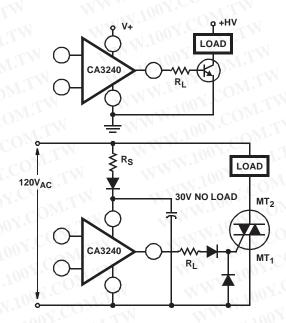


FIGURE 3. METHODS OF UTILIZING THE V<sub>CE</sub> (SAT) SINKING
CURRENT CAPABILITY OF THE CA3240 SERIES

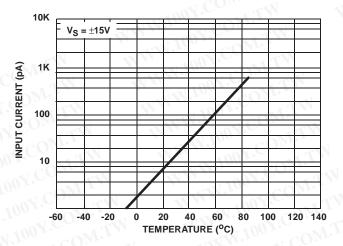


FIGURE 4. INPUT CURRENT vs TEMPERATURE

It is well known that MOSFET devices can exhibit slight changes in characteristics (for example, small changes in input offset voltage) due to the application of large differential input voltages that are sustained over long periods at elevated temperatures.

Both applied voltage and temperature accelerate these changes. The process is reversible and offset voltage shifts of the opposite polarity reverse the offset. In typical linear applications, where the differential voltage is small and symmetrical, these incremental changes are of about the same magnitude as those encountered in an operational amplifier employing a bipolar transistor input stage.

#### Offset-Voltage Nulling

The input offset voltage of the CA3240AE1 and CA3240E1 can be nulled by connecting a  $10k\Omega$  potentiometer between Terminals 3 and 14 or 5 and 8 and returning its wiper arm to Terminal 4, see Figure 5A. This technique, however, gives more adjustment range than required and therefore, a considerable portion of the potentiometer rotation is not fully utilized. Typical values of series resistors that may be placed at either end of the potentiometer, see Figure 5B, to optimize its utilization range are given in the table "Electrical Specifications for Equipment Design" shown on third page of this data sheetAn alternate system is shown in Figure 5C. This circuit uses only one additional resistor of approximately the value shown in the table. For potentiometers, in which the resistance does not drop to  $0\Omega$  at either end of rotation, a value of resistance 10% lower than the values shown in the table should be used.

# **Typical Applications**

#### On/Off Touch Switch

The on/off touch switch shown in Figure 6 uses the CA3240E to sense small currents flowing between two contact points on a touch plate consisting of a PC board metallization "grid". When the "on" plate is touched, current flows between the two halves of the grid causing a positive

shift in the output voltage (Terminal 7) of the CA3240E. These positive transitions are fed into the CA3059, which is used as a latching circuit and zero-crossing TRIAC driver. When a positive pulse occurs at Terminal 7 of the CA3240E, the TRIAC is turned on and held on by the CA3059 and its associated positive feedback circuitry (51k $\Omega$  resistor and 36k $\Omega$ /42k $\Omega$  voltage divider). When the positive pulse occurs at Terminal 1 (CA3240E), the TRIAC is turned off and held off in a similar manner. Note that power for the CA3240E is supplied by the CA3059 internal power supply.

The advantage of using the CA3240E in this circuit is that it can sense the small currents associated with skin conduction while allowing sufficiently high circuit impedance to provide protection against electrical shock.

#### Dual Level Detector (Window Comparator)

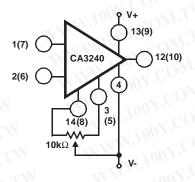
Figure 7 illustrates a simple dual liquid level detector using the CA3240E as the sensing amplifier. This circuit operates on the principle that most liquids contain enough ions in solution to sustain a small amount of current flow between two electrodes submersed in the liquid. The current, induced by an 0.5V potential applied between two halves of a PC board grid, is converted to a voltage level by the CA3240E in a circuit similar to that of the on/off touch switch shown in Figure 6. The changes in voltage for both the upper and lower level sensors are processed by the CA3140 to activate an LED whenever the liquid level is above the upper sensor or below the lower sensor.

#### Constant-Voltage/Constant-Current Power Supply

The constant-voltage/constant-current power supply shown in Figure 8 uses the CA3240E1 as a voltage-error and current-sensing amplifier. The CA3240E1 is ideal for this application because its input common-mode voltage range includes ground, allowing the supply to adjust from 20mV to 25V without requiring a negative supply voltage. Also, the ground reference capability of the CA3240E1 allows it to sense the voltage across the  $1\Omega$  current-sensing resistor in the negative output lead of the power supply. The CA3086 transistor array functions as a reference for both constant-voltage and constant-current limiting. The 2N6385 power Darlington is used as the pass element and may be required to dissipate as much as 40W. Figure 9 shows the transient response of the supply during a 100mA to 1A load transition.

#### **Precision Differential Amplifier**

Figure 10 shows the CA3240E in the classical precision differential amplifier circuit. The CA3240E is ideally suited for biomedical applications because of its extremely high input impedance. To insure patient safety, an extremely high electrode series resistance is required to limit any current that might result in patient discomfort in the event of a fault condition. In this case,  $10M\Omega$  resistors have been used to limit the current to less than  $2\mu A$  without affecting the performance of the circuit. Figure 11 shows a typical electrocardiogram waveform obtained with this circuit.



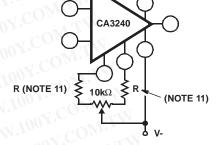


FIGURE 5A. BASIC

FIGURE 5B. IMPROVED RESOLUTION

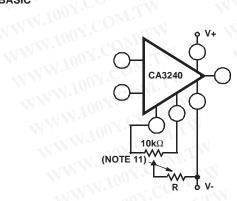
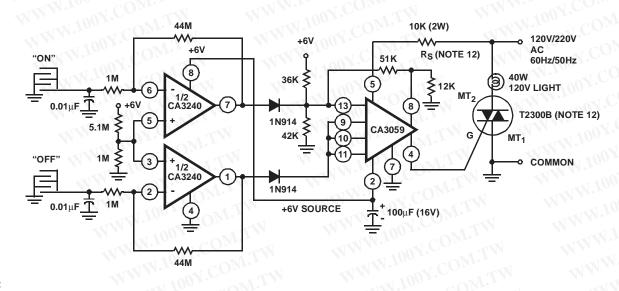


FIGURE 5C. SIMPLER IMPROVED RESOLUTION

#### NOTE:

11. See Electrical Specification Table for value of R.

FIGURE 5. THREE OFFSET-VOLTAGE NULLING METHODS, (CA3240AE1 ONLY)



#### NOTE:

12. At 220V operation, TRIAC should be T2300D, R<sub>S</sub> = 18K, 5W.

FIGURE 6. ON/OFF TOUCH SWITCH

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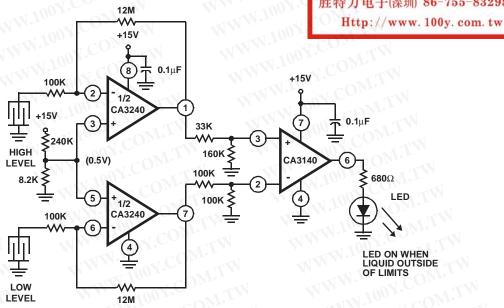


FIGURE 7. DUAL LEVEL DETECTER

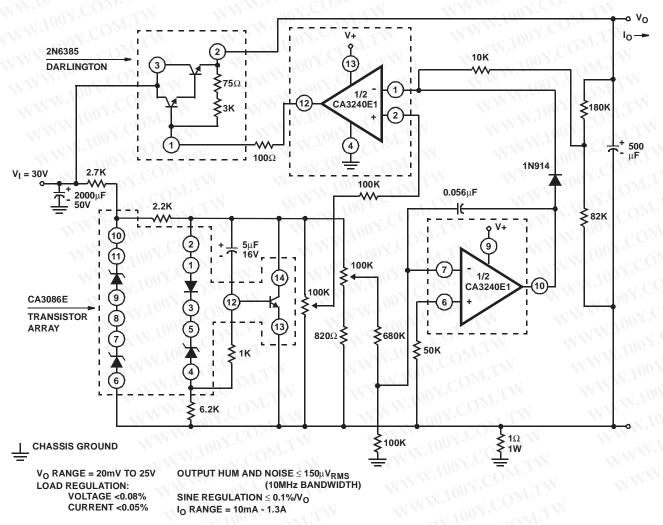
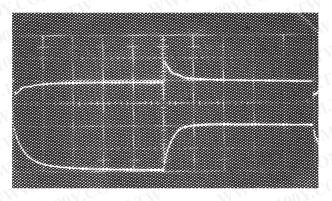


FIGURE 8. CONSTANT-VOLTAGE/CONSTANT-CURRENT POWER SUPPLY



Top Trace: Output Voltage; 500mV/Div., 5µs/Div.

Bottom Trace: Collector Of Load Switching Transistor Load = 100mA to 1A; 5V/Div., 5μs/Div.

#### **FIGURE 9. TRANSIENT RESPONSE**

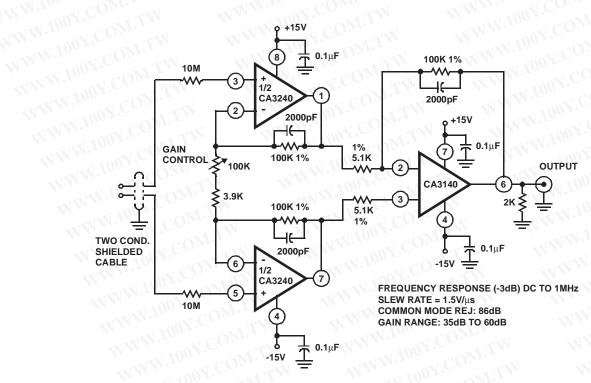
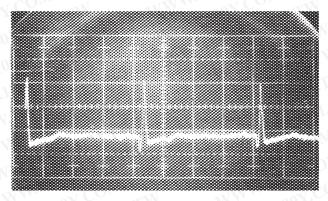


FIGURE 10. PRECISION DIFFERENTIAL AMPLIFIER



Vertical: 1.0mV/Div.

Amplifier Gain = 100X

Scope Sensitivity = 0.1V/Div.

Horizontal: >0.2s/Div. (Uncal)

## FIGURE 11. TYPICAL ELECTROCARIOGRAM WAVEFORM

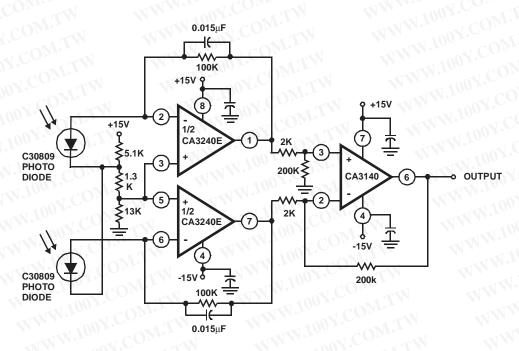


FIGURE 12. DIFFERENTIAL LIGHT DETECTOR

## Differential Light Detector

In the circuit shown in Figure 12, the CA3240E converts the current from two photo diodes to voltage, and applies 1V of reverse bias to the diodes. The voltages from the CA3240E outputs are subtracted in the second stage (CA3140) so that

only the difference is amplified. In this manner, the circuit can be used over a wide range of ambient light conditions without circuit component adjustment. Also, when used with a light source, the circuit will not be sensitive to changes in light level as the source ages.

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# **Typical Performance Curves**

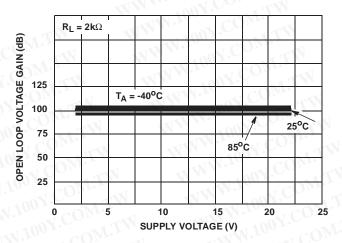


FIGURE 13. OPEN LOOP VOLTAGE GAIN vs SUPPLY VOLTAGE

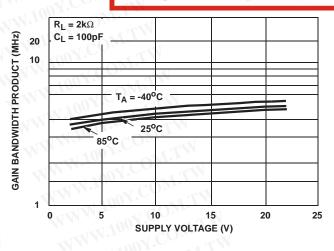


FIGURE 14. GAIN BANDWIDTH PRODUCT vs SUPPLY VOLTAGE

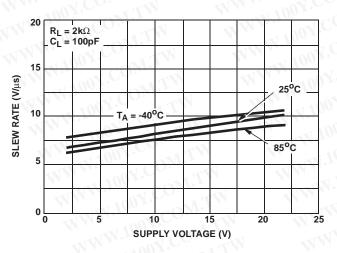


FIGURE 15. SLEW RATE vs SUPPLY VOLTAGE

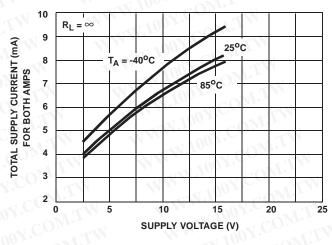


FIGURE 16. QUIESCENT SUPPLY CURRENT vs SUPPLY VOLTAGE

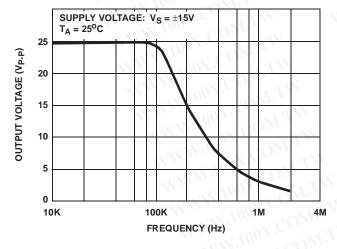


FIGURE 17. MAXIMUM OUTPUT VOLTAGE SWING vs FREQUENCY

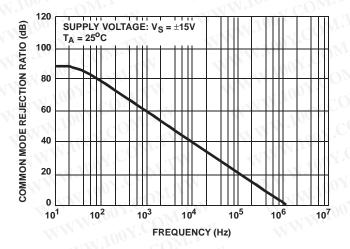


FIGURE 18. COMMON MODE REJECTION RATIO vs FREQUENCY

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## Typical Performance Curves (Continued)

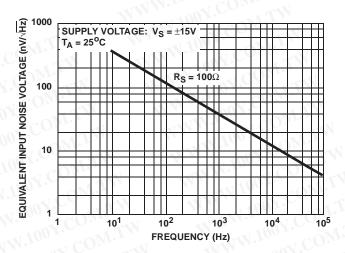


FIGURE 19. EQUIVALENT INPUT NOISE VOLTAGE vs FREQUENCY

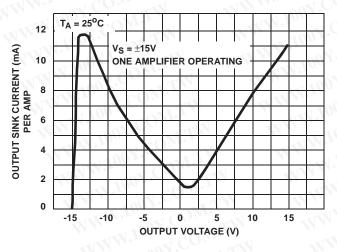


FIGURE 21. OUTPUT SINK CURRENT vs OUTPUT VOLTAGE

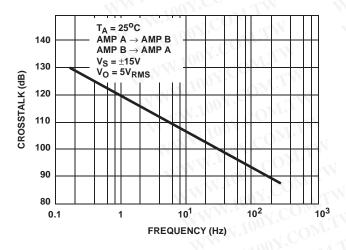


FIGURE 23. CROSSTALK vs FREQUENCY

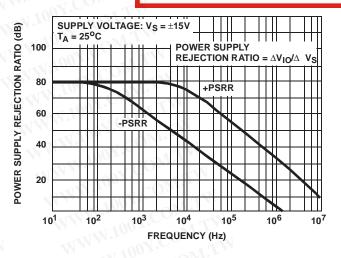


FIGURE 20. POWER SUPPLY REJECTION RATIO vs FREQUENCY

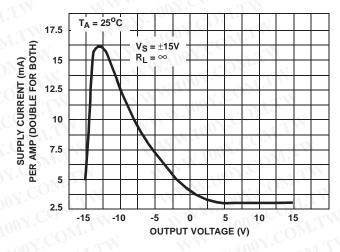


FIGURE 22. SUPPLY CURRENT vs OUTPUT VOLTAGE

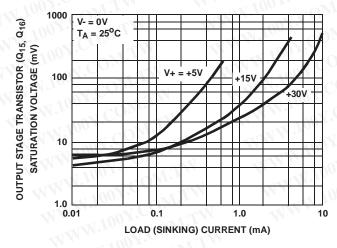
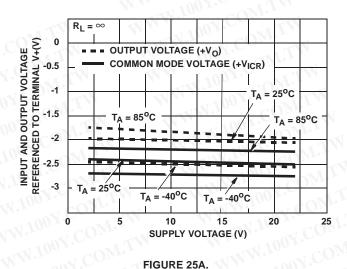


FIGURE 24. VOLTAGE ACROSS OUTPUT TRANSISTORS  $\mathbf{Q}_{15}$  AND  $\mathbf{Q}_{16}$  vs LOAD CURRENT

## Typical Performance Curves (Continued)



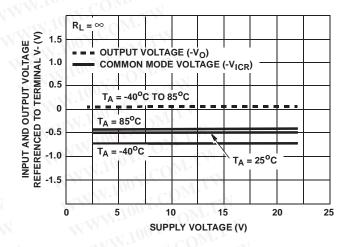
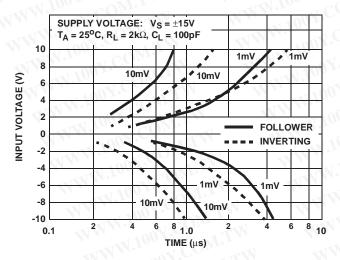


FIGURE 25A. FIGURE 25B.
FIGURE 25. OUTPUT VOLTAGE SWING CAPABILITY AND COMMON MODE INPUT VOLTAGE RANGE vs SUPPLY VOLTAGE



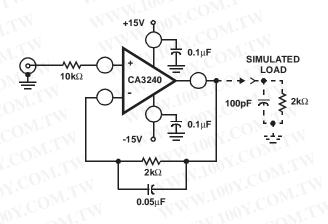


FIGURE 26A. SETTLING TIME vs INPUT VOLTAGE

FIGURE 26B. TEST CIRCUIT (FOLLOWER)

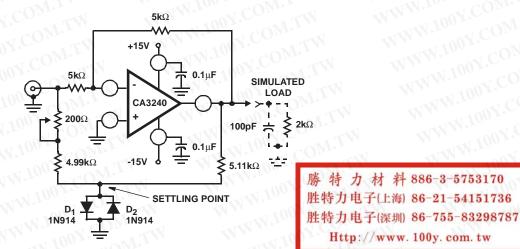


FIGURE 26C. TEST CIRCUIT (INVERTING)
FIGURE 26. INPUT VOLTAGE vs SETTLING TIME

WWW

## Typical Performance Curves (Continued)

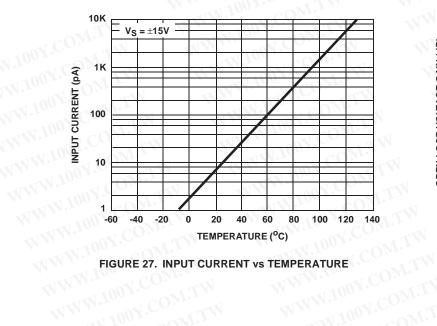


FIGURE 27. INPUT CURRENT vs TEMPERATURE WWW.100Y.CO

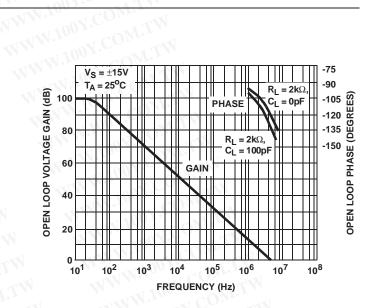


FIGURE 28. OPEN LOOP VOLTAGE GAIN AND PHASE vs **FREQUENCY** WWW.100Y WWW.100Y.COM.T

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