



INA114

Precision INSTRUMENTATION AMPLIFIER

FEATURES

- LOW OFFSET VOLTAGE: 50μV max
- LOW DRIFT: 0.25μV/°C max
- LOW INPUT BIAS CURRENT: 2nA max
- HIGH COMMON-MODE REJECTION:
 115dB min
- INPUT OVER-VOLTAGE PROTECTION: +40V
- WIDE SUPPLY RANGE: ±2.25 to ±18V
- LOW QUIESCENT CURRENT: 3mA max
- 8-PIN PLASTIC AND SOL-16

APPLICATIONS

- BRIDGE AMPLIFIER
- THERMOCOUPLE AMPLIFIER
- RTD SENSOR AMPLIFIER
- MEDICAL INSTRUMENTATION
- DATA ACQUISITION

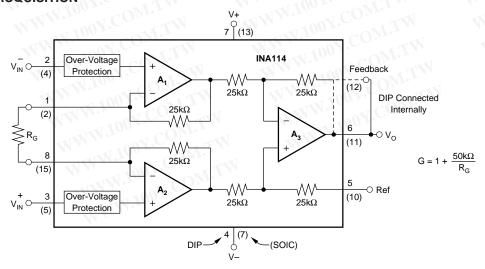
DESCRIPTION

The INA114 is a low cost, general purpose instrumentation amplifier offering excellent accuracy. Its versatile 3-op amp design and small size make it ideal for a wide range of applications.

A single external resistor sets any gain from 1 to 10,000. Internal input protection can withstand up to $\pm 40V$ without damage.

The INA114 is laser trimmed for very low offset voltage (50 μ V), drift (0.25 μ V/°C) and high common-mode rejection (115dB at G = 1000). It operates with power supplies as low as ± 2.25 V, allowing use in battery operated and single 5V supply systems. Quiescent current is 3mA maximum.

The INA114 is available in 8-pin plastic and SOL-16 surface-mount packages. Both are specified for the -40° C to $+85^{\circ}$ C temperature range.



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SPECIFICATIONS

ELECTRICAL

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μs

μs

V

mΑ

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°C/W

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At $T_A = +25$ °C, $V_S = \pm 15$ V, $R_L = 2$ k Ω , unless otherwise noted. INA114BP, BU INA114AP, AU CONDITIONS PARAMETER MIN TYP MAX MIN TYP MAX UNITS INPUT Offset Voltage, RTI $T_A = +25^{\circ}C$ $T_A = T_{MIN}$ to T_{MAX} $\pm 10 + 20/G$ ±50 + 100/G $\pm 25 + 30/G$ 125 + 500/G Initial иV ±0.1 + 0.5/G ±0.25 + 5/G μV/°C vs Temperature $\pm 0.25 + 5/G$ $\pm 1 + 10/G$ vs Power Supply $V_S = \pm 2.25 \text{V to } \pm 18 \text{V}$ 0.5 + 2/G3 + 10/G. μV/V ±0.2 + 0.5/G 10¹⁰ || 6 Long-Term Stability * μV/mo Impedance, Differential * Ω || pF 1010 | 6 Common-Mode * Ω || pF V Input Common-Mode Range +11 +13.5* Safe Input Voltage ±40 ٧ Common-Mode Rejection $V_{CM} = \pm 10V$, $\Delta R_S = 1k\Omega$ G = 180 96 75 90 dΒ G = 1096 115 90 106 dΒ G = 100110 120 106 110 dB G = 1000115 120 106 110 dB **BIAS CURRENT** ±0.5 +2 +5 nA * pA/°C vs Temperature ±8 OFFSET CURRENT ±0.5 ±2 * ±5 nΑ * pA/°C vs Temperature ±8 NOISE VOLTAGE, RTI $G = 1000, R_S = 0\Omega$ f = 10Hz15 * nV/√Hz f = 100Hz11 * nV/√Hz f = 1kHz11 * nV/√Hz $f_B = 0.1Hz$ to 10Hz0.4 * μVp-p Noise Current f=10Hz 0.4 * pA/√Hz pA/√Hz f=1kHz 0.2 $f_B = 0.1Hz$ to 10Hz18 * рАр-р GAIN Gain Equation $1 + (50k\Omega/R_G)$ V/V Range of Gain 10000 * V/V G = 1Gain Error +0.01 ± 0.05 % +0.5 G = 10% +0.02+0.4* G = 100 G = 1000 +0.05+0.5 % * +0.7% +0.5+2 +1 * ±10 ±10 Gain vs Temperature G = 1+2 * ppm/°C 50kΩ Resistance⁽¹⁾ ppm/°C ±25 ±100 Nonlinearity G = 1±0.0001 ±0.001 * ±0.002 % of FSR G = 10±0.0005 ±0.002 * ±0.004 % of FSR G = 100+0.0005±0.002 * ± 0.004 % of FSR ±0.02 % of FSR G = 1000 ± 0.002 ± 0.01 OUTPUT
$$\begin{split} I_O &= 5\text{mA}, \, T_{\text{MIN}} \text{ to } T_{\text{MAX}} \\ V_S &= \pm 11.4 \text{V}, \, R_L = 2 \text{k}\Omega \\ V_S &= \pm 2.25 \text{V}, \, R_L = 2 \text{k}\Omega \end{split}$$
Voltage ±13.5 +13.7* V ±10.5 * +10 * ±1.5 ±1 Load Capacitance Stability 1000 pF Short Circuit Current +20/-15 mA FREQUENCY RESPONSE Bandwidth, -3dB G = 1* MHz G = 10G = 100100 * kH₇ * kH₇ 10 G = 1000kHz 1 $V_0 = \pm 10V, G = 10$ Slew Rate 0.3 0.6 V/us Settling Time, 0.01% G = 118 μs G = 1020 μs G = 100120 * μs

Overload Recovery

TEMPERATURE RANGE

POWER SUPPLY

Voltage Range

Specification Operating

Current

NOTE: (1) Temperature coefficient of the " $50k\Omega$ " term in the gain equation.

G = 1000

50% Overdrive

 $V_{IN} = 0V$

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1100

20

±15 ±2.2

80

+18

±3

85

125

*

*

+2.25

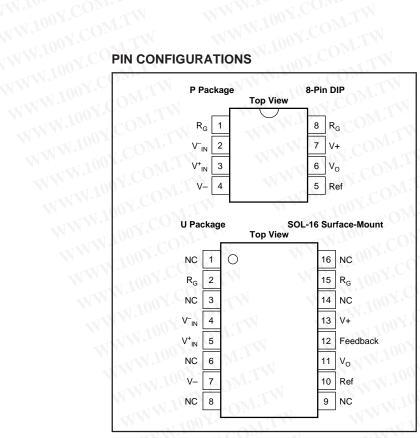
-40

-40



^{*} Specification same as INA114BP/BU.

PIN CONFIGURATIONS



ABSOLUTE MAXIMUM RATINGS(1)

Supply Voltage	±18V
Input Voltage Range	
Output Short-Circuit (to ground)	
Operating Temperature	40°C to +125°C
Storage Temperature	40°C to +125°C
Junction Temperature	+150°C
Lead Temperature (soldering, 10s)	+300°C

NOTE: (1) Stresses above these ratings may cause permanent damage.

ELECTROSTATIC **DISCHARGE SENSITIVITY**

This integrated circuit can be damaged by ESD. Burr-Brown recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

PACKAGE/ORDERING INFORMATION

PRODUCT	PACKAGE	PACKAGE DRAWING NUMBER ⁽¹⁾	TEMPERATURE RANGE
INA114AP	8-Pin Plastic DIP	006	-40°C to +85°C
INA114BP	8-Pin Plastic DIP	006	-40°C to +85°C
INA114AU	SOL-16 Surface-Mount	211	-40°C to +85°C
INA114BU	SOL-16 Surface-Mount	211	-40°C to +85°C

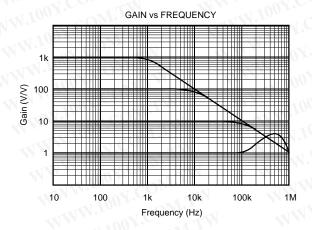
NOTE: (1) For detailed drawing and dimension table, please see end of data sheet, or Appendix C of Burr-Brown IC Data Book.

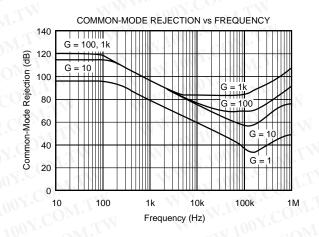
> 特力材料886-3-5753170 胜特力电子(上海) 86-21-54151736 胜特力电子(深圳) 86-755-83298787 Http://www.100y.com.tw

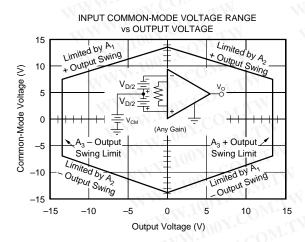
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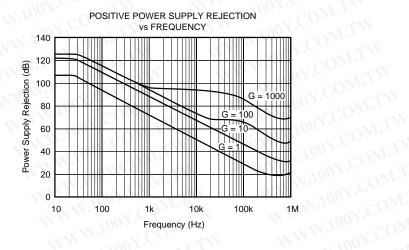
TYPICAL PERFORMANCE CURVES

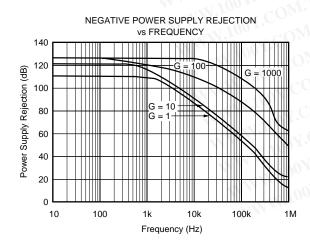
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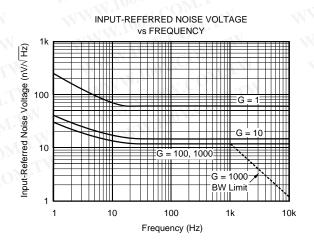








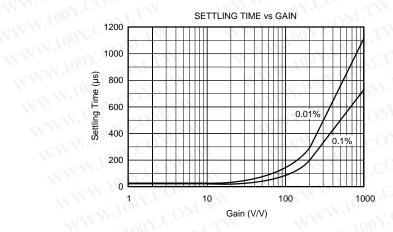


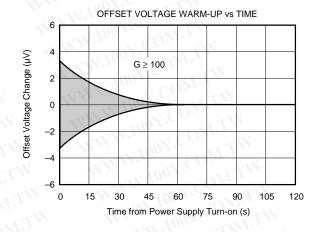


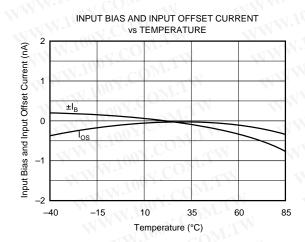


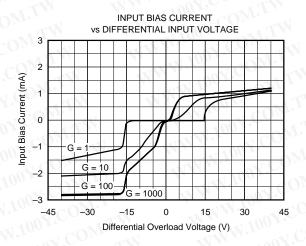
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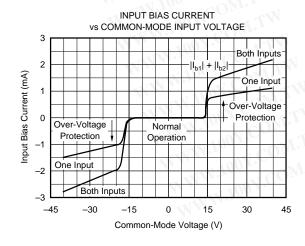
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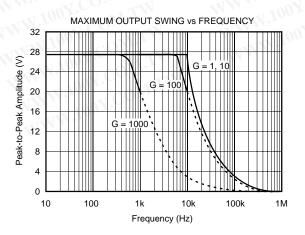






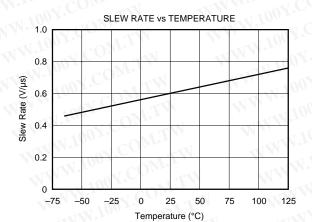


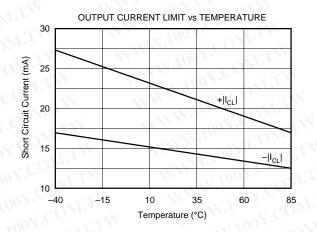


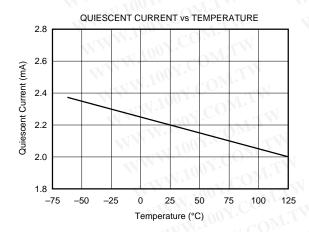


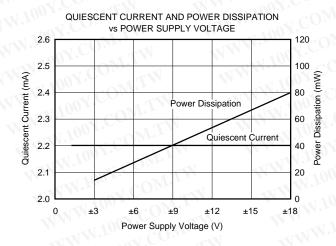
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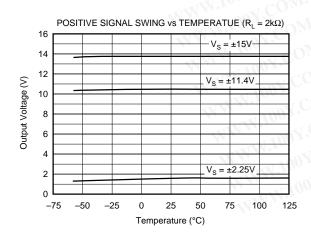
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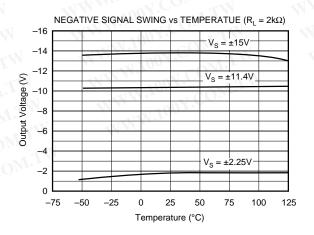








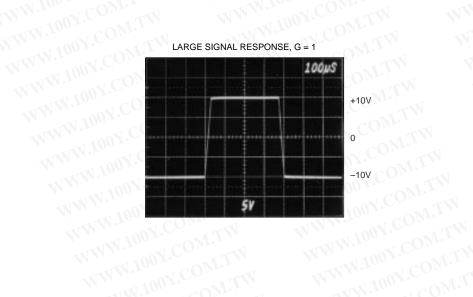




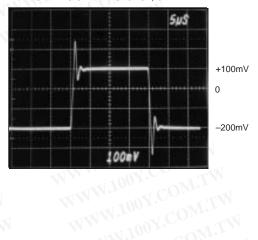


VWW.100Y.COM.TW NW.100Y.CO TYPICAL PERFORMANCE CURVES (CONT) WWW.100Y.

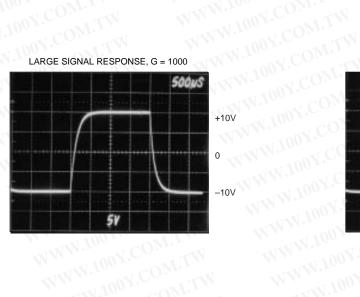
At $T_A = +25$ °C, $V_S = \pm 15$ V, unless otherwise noted. WWW.100Y.CONT.



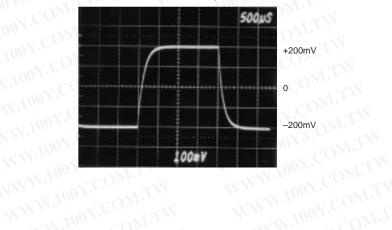
SMALL SIGNAL RESPONSE, G = 1



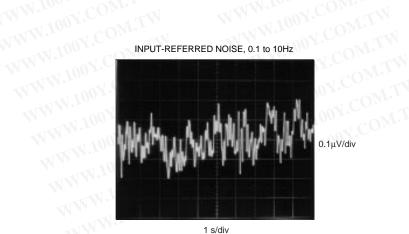
WWW.100Y.COM.TW WWW.100Y.COM.TW LARGE SIGNAL RESPONSE, G = 1000



SMALL SIGNAL RESPONSE, G = 1000



WWW.100Y.COM.TW MW.100X.COM.TW



APPLICATION INFORMATION

Figure 1 shows the basic connections required for operation of the INA114. Applications with noisy or high impedance power supplies may require decoupling capacitors close to the device pins as shown.

The output is referred to the output reference (Ref) terminal which is normally grounded. This must be a low-impedance connection to assure good common-mode rejection. A resistance of 5Ω in series with the Ref pin will cause a typical device to degrade to approximately 80dB CMR (G = 1).

SETTING THE GAIN

Gain of the INA114 is set by connecting a single external resistor, $R_{\rm G}$:

$$G = 1 + \frac{50 \text{ k}\Omega}{R_G} \tag{1}$$

Commonly used gains and resistor values are shown in Figure 1.

The $50k\Omega$ term in equation (1) comes from the sum of the two internal feedback resistors. These are on-chip metal film resistors which are laser trimmed to accurate absolute val-

ues. The accuracy and temperature coefficient of these resistors are included in the gain accuracy and drift specifications of the INA114.

The stability and temperature drift of the external gain setting resistor, R_G , also affects gain. R_G 's contribution to gain accuracy and drift can be directly inferred from the gain equation (1). Low resistor values required for high gain can make wiring resistance important. Sockets add to the wiring resistance which will contribute additional gain error (possibly an unstable gain error) in gains of approximately 100 or greater.

NOISE PERFORMANCE

The INA114 provides very low noise in most applications. For differential source impedances less than $1k\Omega$, the INA103 may provide lower noise. For source impedances greater than $50k\Omega$, the INA111 FET-input instrumentation amplifier may provide lower noise.

Low frequency noise of the INA114 is approximately $0.4\mu Vp$ -p measured from 0.1 to 10Hz. This is approximately one-tenth the noise of "low noise" chopper-stabilized amplifiers.

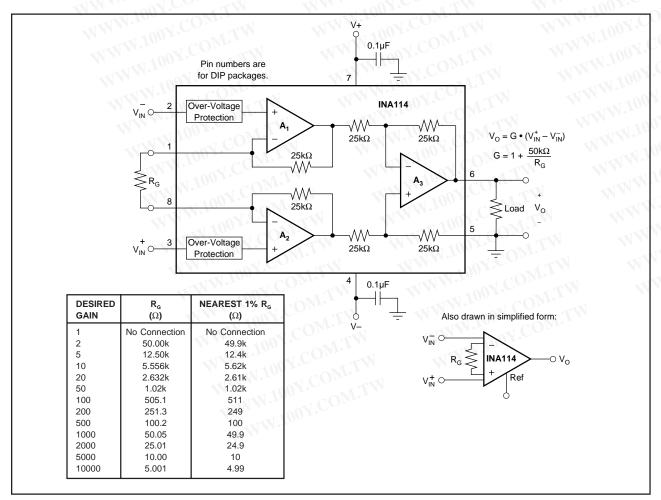


FIGURE 1. Basic Connections.



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OFFSET TRIMMING

The INA114 is laser trimmed for very low offset voltage and drift. Most applications require no external offset adjustment. Figure 2 shows an optional circuit for trimming the output offset voltage. The voltage applied to Ref terminal is summed at the output. Low impedance must be maintained at this node to assure good common-mode rejection. This is achieved by buffering trim voltage with an op amp as shown.

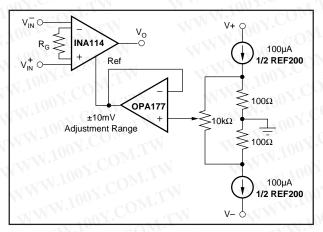


FIGURE 2. Optional Trimming of Output Offset Voltage.

INPUT BIAS CURRENT RETURN PATH

The input impedance of the INA114 is extremely high—approximately $10^{10}\Omega$. However, a path must be provided for the input bias current of both inputs. This input bias current is typically less than ± 1 nA (it can be either polarity due to cancellation circuitry). High input impedance means that this input bias current changes very little with varying input voltage.

Input circuitry must provide a path for this input bias current if the INA114 is to operate properly. Figure 3 shows various provisions for an input bias current path. Without a bias current return path, the inputs will float to a potential which exceeds the common-mode range of the INA114 and the input amplifiers will saturate. If the differential source resistance is low, bias current return path can be connected to one input (see thermocouple example in Figure 3). With higher source impedance, using two resistors provides a balanced input with possible advantages of lower input offset voltage due to bias current and better common-mode rejection.

INPUT COMMON-MODE RANGE

The linear common-mode range of the input op amps of the INA114 is approximately ± 13.75 V (or 1.25V from the power supplies). As the output voltage increases, however, the linear input range will be limited by the output voltage swing of the input amplifiers, A_1 and A_2 . The common-mode range is related to the output voltage of the complete amplifier—see performance curve "Input Common-Mode Range vs Output Voltage."

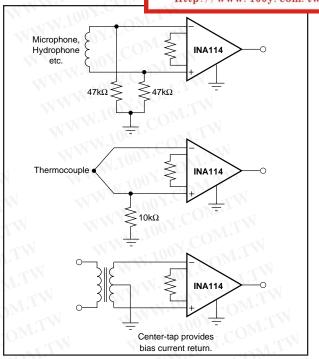


FIGURE 3. Providing an Input Common-Mode Current Path.

A combination of common-mode and differential input signals can cause the output of A₁ or A₂ to saturate. Figure 4 shows the output voltage swing of A₁ and A₂ expressed in terms of a common-mode and differential input voltages. Output swing capability of these internal amplifiers is the same as the output amplifier, A₃. For applications where input common-mode range must be maximized, limit the output voltage swing by connecting the INA114 in a lower gain (see performance curve "Input Common-Mode Voltage Range vs Output Voltage"). If necessary, add gain after the INA114 to increase the voltage swing.

Input-overload often produces an output voltage that appears normal. For example, an input voltage of +20V on one input and +40V on the other input will obviously exceed the linear common-mode range of both input amplifiers. Since both input amplifiers are saturated to nearly the same output voltage limit, the difference voltage measured by the output amplifier will be near zero. The output of the INA114 will be near 0V even though both inputs are overloaded.

INPUT PROTECTION

The inputs of the INA114 are individually protected for voltages up to ± 40 V. For example, a condition of -40V on one input and +40V on the other input will not cause damage. Internal circuitry on each input provides low series impedance under normal signal conditions. To provide equivalent protection, series input resistors would contribute excessive noise. If the input is overloaded, the protection circuitry limits the input current to a safe value (approximately 1.5mA). The typical performance curve "Input Bias Current vs Common-Mode Input Voltage" shows this input

current limit behavior. The inputs are protected even if no power supply voltage is present.

OUTPUT VOLTAGE SENSE (SOL-16 package only)

The surface-mount version of the INA114 has a separate output sense feedback connection (pin 12). Pin 12 must be connected to the output terminal (pin 11) for proper operation. (This connection is made internally on the DIP version of the INA114.)

The output sense connection can be used to sense the output voltage directly at the load for best accuracy. Figure 5 shows how to drive a load through series interconnection resistance. Remotely located feedback paths may cause instability. This can be generally be eliminated with a high frequency feedback path through C₁. Heavy loads or long lines can be driven by connecting a buffer inside the feedback path (Figure 6).

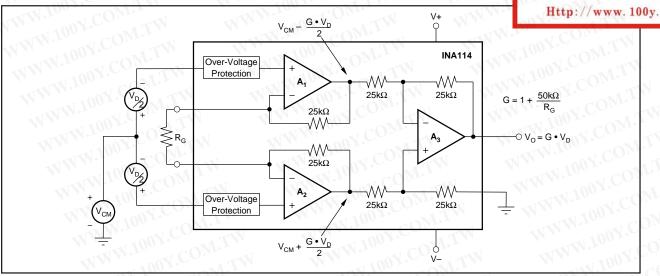


FIGURE 4. Voltage Swing of A₁ and A₂.

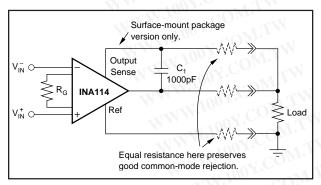


FIGURE 5. Remote Load and Ground Sensing.

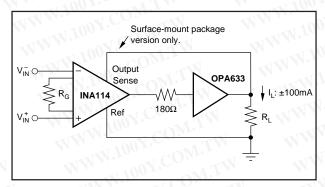


FIGURE 6. Buffered Output for Heavy Loads.

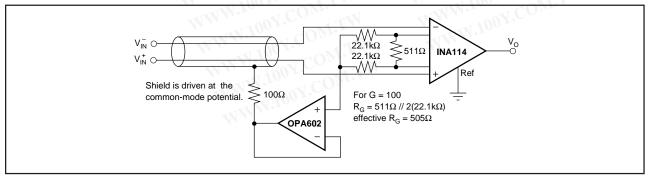


FIGURE 7. Shield Driver Circuit.



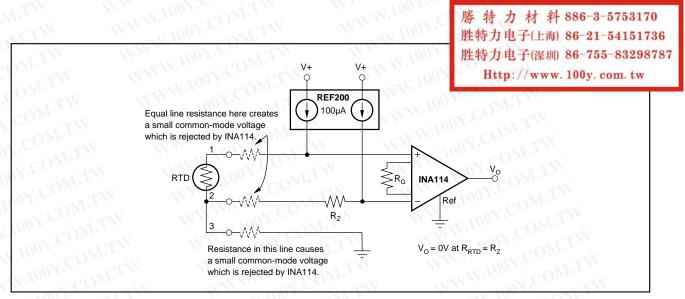


FIGURE 8. RTD Temperature Measurement Circuit.

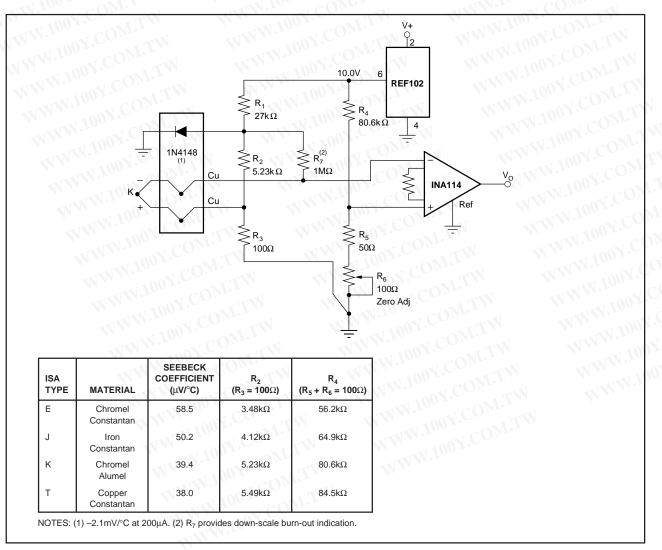


FIGURE 9. Thermocouple Amplifier With Cold Junction Compensation.

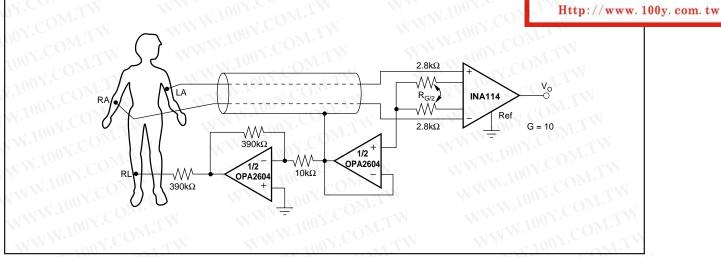


FIGURE 10. ECG Amplifier With Right-Leg Drive.

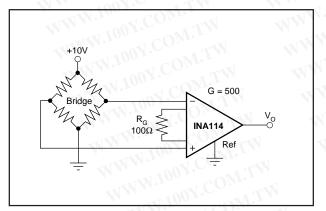


FIGURE 11. Bridge Transducer Amplifier.

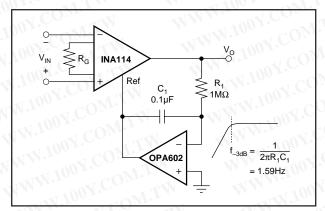


FIGURE 12. AC-Coupled Instrumentation Amplifier.

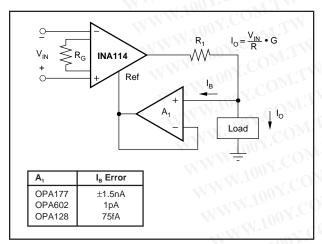


FIGURE 13. Differential Voltage-to-Current Converter.